## BEAVERTON SCHOOL DISTRICT FIVE OAKS MIDDLE SCHOOL

1600 NW 173<sup>rd</sup> Ave, Beaverton, OR 97006

## SEISMIC EVALUATION AND CONCEPTUAL SEISMIC STRENGTHENING SCHEME April 20, 2022



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Project No. 21603.10

## 1 INTRODUCTION AND PROJECT SUMMARY

Holmes Structures has been engaged by Beaverton School District to perform a seismic evaluation of the Five Oaks Middle School located at 1600 NW 173<sup>rd</sup> Ave, Beaverton, OR 97006. American Society of Civil Engineers (ASCE) Standard 41-17, Seismic Evaluation and Retrofit of Existing Buildings was used to complete the evaluation and strengthening scheme using the Tier 1 seismic evaluation procedure. The purpose of this report is to present the seismic deficiencies of the building only. Any issues related to gravity system not associated with the lateral resisting system will not be addressed in this report.

A strengthening scheme is included in this report, which provides recommendations for rehabilitation of the deficiencies found during the Tier 1 evaluation.

A summary of the project and building parts is found in the table below. A site plan showing the buildings and its different components is shown in Figures 1 and 2.

Project Summary Information						
Building Part	Building Name	Included in Retrofit	Year Built	Building Type	Nonstructural Retrofits Included in Scope Y/N	Previous Seismic Retrofit Y/N (Year if Yes)
А	Gym	У	1974	PC1	У	Ν
В	Classrooms	У	1974	RM1	У	Ν
С	Classrooms	У	1974	RM1	У	Ν
D	Covered Play Area	У	1989	S3	У	Ν
E	Classroom Additions	Ν	2019	S2A	Ν	Ν
Total Retrofit Cost					\$11,010,338	
Retrofit Square Feet					152,276	
Retrofit Cost Per Square Foot					\$70.91	
Is the sch	Is the school within a tsunami, FEMA flood zone or other high hazard area? No *				No *	

#### Table 1: Project Summary Information

\* The site is partially in a Moderate liquefaction zone and partially in a Moderate landsliding zone, per DOGAMI mapping. However the site-specific geotechnical report for the 2019 classroom included a liquefaction analysis and concluded that there is low risk of liquefaction at this site. The 2019 geotechnical report also concluded that there is low risk of earthquake-induced landsliding at this site.



Engir	Engineering Report Checklist			
$\boxtimes$	Engineering Report Cover Page			
$\boxtimes$	Project Summary Page	Page 1		
$\boxtimes$	Building Parts Identification	Page 3		
$\boxtimes$	Statement of the Performance Objective	Page 7		
	Summary of Deficiencies	Page 10		
$\boxtimes$	Structural Seismic Deficiencies	Page 10		
$\boxtimes$	Nonstructural Seismic Deficiencies	Page 13		
	Summary of Mitigation/Retrofit	Page 15		
$\boxtimes$	Structural Mitigation/Retrofit	Page 15		
$\boxtimes$	Nonstructural Mitigation/Retrofit	Page 17		
	Summary Construction Cost Estimate	Page 19		
$\boxtimes$	Direct Cost	Page 19		
$\boxtimes$	Indirect Soft Cost	Page 19		
$\boxtimes$	Certification Statement by Engineer	Page 19		
	ASCE 41-17 Tier 1 Checklists	Page 20		
$\boxtimes$	Basic Configuration Checklist	Page 21		
$\boxtimes$	Building System Structural Checklists	Page 29		
$\boxtimes$	Nonstructural Checklist	Page 38		
$\boxtimes$	Retrofit Drawings & Sketches	Page 44		
$\boxtimes$	Itemized Construction Cost Estimate	Page 69		

#### Table 2: Engineering Report Checklist

#### 2 LIMITATIONS

Findings presented as a part of this project are for the sole use of Beaverton School District in its evaluation of the subject property. The findings are not intended for use by other parties and may not contain sufficient information for the purposes of other parties or other uses. Our professional services are performed using a degree of care and skill normally exercised, under similar circumstances, by reputable consultants practicing in this field at this time. No other warranty, expressed or implied, is made as to the professional advice presented in this report.

No material sampling or destructive testing has been undertaken. Our conclusions are based on our review of the original building drawings as available, our visual observations and experience with buildings of this type.



### 3 BUILDING PARTS IDENTIFICATION



Figure 1: Building Year Plan

Five Oaks Middle School is comprised of three eras of construction. The majority of the building was constructed in 1974 and consists of the gym (Part A) and classroom areas (Parts B and C), which have a 1 inch expansion joint between them. In 1989 a covered play area (Part D) was added outside the northeast end of the gym, and in 2019 two classroom blocks (Part E) were added at the northwest end of the school building with a 4 inch seismic gap.





Figure 2: Building Parts

### 1974 Gym (Part A)

The gym is a tilt-up concrete structure and was constructed as part of the original building circa 1974. It was designed by Hewlett, Jamison & Atkinson Architects and the Engineer who stamped the structural drawings was Robert A Walker.

The Gym building contains a main gym and a secondary gym separated by a locker room block which also has a mezzanine floor above. It is rectangular in plan with approximately 25,000 sf of floor area, including the mezzanine. The perimeter walls are precast concrete tilt-up panels connected by insitu concrete pilasters, which protrude on the exterior of the gym. There are also interior tilt-up walls on both sides of the mezzanine, extending up to the gym roof. The roof is 22 GA. metal deck supported by long-span steel truss joists at 8 ft o.c., spanning between exterior and interior tilt-up walls. Some roof joists bear onto the pilasters, however some bear onto pockets in the tilt-up panels. The mezzanine floor is a 3 ½ inch concrete slab, supported by steel truss joists at 4 ft o.c., spanning between tilt-up walls and an interior steel beam and columns. The foundations at the tilt-up walls are typically 4 ft wide concrete strip footings, however the tilt-up walls are not connected to the footings.

The lateral system at the Gym building consists of the metal deck diaphragm at the roof and the concrete slab diaphragm at the mezzanine, which distribute lateral forces to the perimeter and interior tilt-up walls, which act as shear walls to transfer the lateral forces down to the foundations.



### 1974 School Building (Parts B and C)

The School Building (Parts B and C) are reinforced masonry shear wall structures constructed along with the gym circa 1974. They were designed by Hewlett, Jamison & Atkinson Architects and the Engineer who stamped the structural drawings was Robert A Walker. Part B is structural separated from Part A by a 1 inch expansion joint. Parts B and C are themselves separated by a 1 inch expansion joint.

Part B contains the kitchen/cafeteria/commons areas, performing arts, computer lab, vocational and special education areas, and the main admin offices. It is irregular in plan with approximately 56,000 sf of floor area. There is a small mezzanine above the performing arts area the connects to the gym, and several elevated mechanical rooms. Part C predominantly contains classrooms, as well as science labs and the media/resource center. It is irregular in plan with approximately 66,000 sf of floor area. There are several elevated mechanical rooms. The typical roof height is approximately 17 ft, with popup roofs at the mechanical rooms. Above the commons and admin areas in Part B, the roof height is approximately 27 ft.

A renovation project was performed at Parts B and C circa 2019. However this renovation did not include any major structural work or seismic retrofit.

The roof structure at Parts B and C is metal deck supported by long-span steel truss joists at 8 ft o.c., spanning typically between exterior 8 inch reinforced masonry walls and interior steel beams supported on steel columns. There are also some interior reinforced masonry walls. Most of the masonry walls are partially grouted with vertical reinforcing at 48 inches o.c. Some walls are solid grouted and in several locations the walls are reinforced concrete rather than masonry. The foundations at the masonry walls are typically 2 ft wide concrete strip footings, with spread footings at the interior steel columns.

The lateral system at Parts B and C consists of the metal deck diaphragm at the roof which distributes lateral forces to the perimeter and interior reinforced masonry walls, which act as shear walls to transfer the lateral forces down to the foundations. The vertical reinforcing bars in the walls are dowelled into the foundations.

Note that the metal deck roof diaphragm is 22 GA typically, however at the high roof areas above the commons and admin offices it is 18 GA.

### 1989 Covered Play Area (Part D)

The covered play area is a lightweight steel canopy designed by Dull Olson Weeks Architects. Structural drawings were not available for our review.

This open canopy structure is square in plan with 8,100 sf of floor area. The roof height is approximately 20 ft. The roof is metal deck supported on light gauge metal purlins, which span between steel portal frames. The latera system is steel moment frames in both directions. The foundations are indicated as concrete spread footings at the steel portal frame legs.

#### 2019 Classroom Additions (Part E)

This Building Part is newly constructed and is not in scope.







Picture 1: Building Part A

Picture 2: Building Part B



Picture 3: Building Part C

Picture 4: Building Part D





Picture 7: Gym Beam Framing

Picture 8: Locker Rooms



Picture 7: Typ. Corridor

Picture 8: Interior

#### 4 STATEMENT OF PERFORMANCE OBJECTIVE

Five Oaks Middle School was evaluated in accordance with ASCE 41-17, the national standard for evaluating and retrofitting existing buildings, using its Tier 1 evaluation procedure. A Tier 1 evaluation uses checklists to coarsely but systematically identify or screen areas of potential seismic deficiencies. Structural systems or components which are identified as "non-compliant" (NC) should be further evaluated using a more detailed Tier 2 or Tier 3 evaluation to confirm if an actual deficiency exists and quantify the extent or severity. Tier 2 or Tier 3 evaluations were beyond the scope of this project.

See Figure 3 below for a summary of basic performance objectives for existing buildings according to ASCE 41-17. The target performance objective for existing buildings (BPOE) for Building Parts A and B, which are assumed to be Risk Category IV structures, is to achieve Life Safety (S-3) Structural Performance Level for BSE-2E seismic event and Immediate Occupancy (S-1) Structural Performance Level for a BSE-1E seismic event. The BPOE for Building Parts C and D, which are assumed to be Risk Category III structures, is to achieve Limited Safety (S-4) Structural Performance Level for BSE-2E seismic event. The BSE-1E hazard is not explicitly checked as part of the Tier 1 structural procedure for this Risk Category. The nonstructural target for Building Parts A



and B is Hazard Reduction (HR) and Position Retention (PR) for the BSE-2E and BSE-1E hazard respectively. For Building Parts C and D the nonstructural target is HR at the BSE-2E hazard.

The BSE-1E and BSE-2E hazard for the site is presented in Table 3 below. Site Class D was assumed for the site.

a	able 3: ASCE41 Tier 1 Hazard Parameter		
		BSE-1E	BSE-2E
	S <sub>xs</sub>	0.380g	0.820g
	S <sub>X1</sub>	0.206g	0.586g

The site is classified as having a High Level of Seismicity per ASCE 41-17 Table 2-4.



Figure 3: Basic Performance Objective for Existing Buildings (BPOE)



### 5 OBSERVATIONS

### 5.1 Site Survey

Holmes and Oh Planning & Design conducted a site survey of the Five Oaks Middle School on 2/11/2022 to verify the general conformance of the existing documents and general building conditions. The existing drawings appear to be generally accurate based on the visual observations of the accessible building areas.

#### 5.2 Documents Reviewed

The following documents were provided and reviewed for this project:

- Architectural drawings for "Beaverton Intermediate School No. 6", prepared by Hewlett Jamison & Atkinson Architects, dated 1974
- Structural drawings for "Beaverton Intermediate School No. 6", stamped by Robert A. Walker, Registered Professional Engineer, dated 1974
- Architectural drawing for "Five Oaks Intermediate School, Covered Play Addition", prepared by Dull Olson Weeks, dated 1989
- Architectural drawings for "Five Oaks Middle School Renovation", prepared by Bassetti Architects, record set dated April 16, 2021.
- Structural drawings for "Five Oaks Middle School Renovation", prepared by Catena Consulting Engineers, record set dated December 4, 2020.



## 6 SUMMARY OF DEFICIENCIES

The seismic structural and nonstructural deficiencies are listed in tables below for each building part. The deficiency identification tag noted in the tables below corresponds with the seismic retrofit tag in Section 7 and in the seismic strengthening scheme. The tags are also used in the cost estimate for complete tracking of each deficiency, corresponding retrofit and associated cost.

TAG	Deficiency/unknown	Description
F1	Inadequate connections between tilt-up wall panels and foundations	The walls are not doweled into the foundations, therefore there is no direct load path for in-plane shear forces in the walls to transfer to foundations.
F5, R9	Inadequate out-of-plane strength at tilt-up wall at northwest of gym	The 1 inch expansion gap between Part A and Part B is inadequate, therefore the roof beam at Part B will impose an out-of-plane load on the tilt-up wall, which the wall does not have adequate strength to resist.
M1, M2, M3, R10	Inadequate seismic separation between Part A and Part B	The 1 inch expansion gap between Part A and Part B is inadequate, therefore the mezzanine at Part B will impose seismic loads on Part A. However the existing load paths and connections to transfer these loads are not adequate.
M4	Inadequate connections between mezzanine floor and tilt-up walls	The mezzanine truss joists are not connected to the walls.
R1	Inadequate out-of-plane connections between gym roof and end walls.	The roof truss joists are not connected to the tilt-up walls at each end of the gym, to provide out-of-plane support to the walls.
R2	Inadequate out-of-plane connections between gym roof and side walls.	The tilt-up walls at the sides of the gym do not have connections to the roof framing, to provide out-of-plane support to the walls.
R3	Inadequate capacity at roof diaphragm	The metal deck at the roof does not have adequate strength to distribute in-plane forces from the roof to the walls.
R8	Inadequate connections between metal deck and steel framing at roof	The metal deck at the roof is not adequately welded to the steel framing.

### 6.1 Building Part A Structural Seismic Deficiencies



TAG	Deficiency/unknown	Description
F2, F8	Insufficient shear walls	The lengths and locations of the existing masonry shear walls are not adequate in some areas of the building. As a result, some existing walls are overstressed. In other areas the roof structure is not adequate to drag seismic forces long distances to the existing shear walls.
F3	Insufficient footings.	Footings are inadequate at some shear walls
M1, M2, M3	Inadequate seismic separation between Part B and Part A	The 1 inch expansion gap between Part B and Part A is inadequate, therefore the mezzanine at Part B will impose seismic loads on Part A. However the existing load paths and connections to transfer these loads are not adequate.
R5	Inadequate out-of-plane connections between roof and masonry walls	Where the roof trusses run parallel to the masonry walls, no connections exist to tie the tops of the walls to the roof structure for out-of-plane support of the walls.
R6, R7	Inadequate drag ties at roof diaphragm	In some locations, existing drag members and connections are inadequate or are not provided, to collect in-plane forces and transfer these to the shear walls.
R8	Inadequate connections between metal deck and steel framing at roof	The metal deck at the roof is not adequately welded to the steel framing.
R11, R12	Inadequate seismic separation between Part B and Part A	The 1 inch expansion gap between Part B and Part A is inadequate, therefore the roof at Part B will impose seismic loads on Part A. However the existing load paths and connections to transfer these loads are not adequate.
R13	Inadequate out-of-plane connections at exterior wall	At the main entry area on the southwest side of the building, the existing connections between the masonry wall and the roof are assumed to be inadequate.

#### 6.2 Building Part B Structural Seismic Deficiencies



TAG	Deficiency/unknown	Description
F2, F8	Insufficient shear walls	The lengths and locations of the existing masonry shear walls are not adequate in some areas of the building. As a result, some existing walls are overstressed. In other areas the roof structure is not adequate to drag seismic forces long distances to the existing shear walls.
F3	Insufficient footings.	Footings are inadequate at some shear walls
R5	Inadequate out-of-plane connections between roof and masonry walls	Where the roof trusses run parallel to the masonry walls, no connections exist to tie the tops of the walls to the roof structure for out-of-plane support of the walls.
R6, R7	Inadequate drag ties at roof diaphragm	In some locations, existing drag members and connections are inadequate or are not provided, to collect in-plane forces and transfer these to the shear walls.
R8	Inadequate connections between metal deck and steel framing at roof	The metal deck at the roof is not adequately welded to the steel framing.

### 6.3 Building Part C Structural Seismic Deficiencies

## 6.4 Building Part D Structural Seismic Deficiencies

TAG	Deficiency/unknown	Description
F6	Insufficient anchor bolts at portal frame legs	The existing anchor bolts are not adequate.
F7	Insufficient strength at portal frame moment connections	The existing connections are not adequate.



TAG	Deficiency/unknown	Description
N2	Masonry walls in locker room	Tops of walls are not adequately braced for o-o-p forces.
N3	Fire Suppression piping	Bracing is inadequate
N4	Lay-in tile ceilings (at mezzanine)	Bracing is inadequate
N5	Other interior walls and partitions	Bracing is inadequate
N6	Tall Narrow Contents	Bracing is inadequate
N7	Fall-prone Contents over 20 lbs	Bracing is inadequate
N8	Fall-prone Equipment over 20 lbs	Bracing is inadequate
N9	Tall Narrow Equipment over 6 ft high	Bracing is inadequate
N10	In-Line Equipment over 75 lb	Bracing is inadequate
N11	Conduit Couplings	Couplings are inadequate
N12	Couplings for Fluid and Gas Pipe	Couplings are inadequate
N13	Gas shut-off valve	Not provided
N14	Fluid and Gas Piping	Bracing is inadequate
N15	Ducts Larger than 6 sf of Cross-Section	Bracing is inadequate

### 6.5 Building Part A Nonstructural Seismic Deficiencies

### 6.6 Building Part B Nonstructural Seismic Deficiencies

TAG	Deficiency/unknown	Description
N3	Fire Suppression piping	Bracing is inadequate
N4	Lay-in tile ceilings	Bracing is inadequate
N5	Other interior walls and partitions	Bracing is inadequate
N6	Tall Narrow Contents	Bracing is inadequate
N7	Fall-prone Contents over 20 lbs	Bracing is inadequate
N8	Fall-prone Equipment over 20 lbs	Bracing is inadequate
N9	Tall Narrow Equipment over 6 ft high	Bracing is inadequate
N10	In-Line Equipment over 75 lb	Bracing is inadequate
N11	Conduit Couplings	Couplings are inadequate
N12	Couplings for Fluid and Gas Pipe	Couplings are inadequate
N13	Gas shut-off valve	Not provided
N14	Fluid and Gas Piping	Bracing is inadequate
N15	Ducts Larger than 6 sf of Cross-Section	Bracing is inadequate



TAG	Deficiency/unknown	Description
N1	Brick pilasters at corridors	Bracing is inadequate
N3	Fire Suppression piping	Bracing is inadequate
N5	Other interior walls and partitions	Bracing is inadequate
N6	Tall Narrow Contents	Bracing is inadequate
N7	Fall-prone Contents over 20 lbs	Bracing is inadequate
N8	Fall-prone Equipment over 20 lbs	Bracing is inadequate
N9	Tall Narrow Equipment over 6 ft high	Bracing is inadequate
N10	In-Line Equipment over 75 lb	Bracing is inadequate

## 6.7 Building Part C Nonstructural Seismic Deficiencies

## 6.8 Building Part D Nonstructural Seismic Deficiencies

No deficiencies were noted.



## 7 SUMMARY OF MITIGATION/RETROFIT

## 7.1 Building Part A Structural Seismic Retrofit

#	Deficiency/unknown	Description
F1	Inadequate connections between tilt-up wall panels and foundations	Provide new reinforced concrete band at base of tilt-up walls, with rebars epoxy dowelled into existing walls and foundations.
F5, R9	Inadequate out-of-plane strength at tilt-up wall at northwest of gym	Provide new steel strongback to span vertically and support the wall for out-of-plane forces. Provide struts at top of wall to tie into gym roof structure.
M1, M2, M3, R10	Inadequate seismic separation between Part A and Part B	Provide new connections to tie the mezzanine structure to the gym structure. Provide new strut to tie the Part A roof structure to the gym walls.
M4	Inadequate connections between mezzanine floor and tilt-up walls	Provide new connections to tie the mezzanine floor to the tilt- up walls.
R1	Inadequate out-of-plane connections between gym roof and end walls.	Provide new out-of-plane connections.
R2	Inadequate out-of-plane connections between gym roof and side walls.	Provide new out-of-plane connections and continuity ties across gym roof.
R3	Inadequate capacity at roof diaphragm	Provide new horizontal steel channel X-bracing at the underside of the roof.
R8	Inadequate connections between metal deck and steel framing at roof	Provide additional welding of metal deck to the steel framing (this will require removing and replacing the roofing)



TAG	Deficiency/unknown	Description
F2, F8	Insufficient shear walls	Provide new reinforced masonry shear walls in selected locations
F3	Insufficient footings.	Provide new or supplemental foundations.
M1, M2, M3	Inadequate seismic separation between Part B and Part A	Provide new connections to tie the P{art B mezzanine structure to the gym structure.
R5	Inadequate out-of-plane connections between roof and masonry walls	Provide new out-of-plane connections and continuity ties to develop adequate sub diaphragms.
R6, R7	Inadequate drag ties at roof diaphragm	Provide new drag members and connections.
R8	Inadequate connections between metal deck and steel framing at roof	Provide additional welding of metal deck to steel framing (this will require removing and replacing the roofing)
R11, R12	Inadequate seismic separation between Part B and Part A	Provide new connections to tie the Part B roof structure to the gym structure.
R13	Inadequate out-of-plane connections at exterior wall	Provide new out-of-plane connections

### 7.2 Building Part B Structural Seismic Retrofit

## 7.3 Building Part C Structural Seismic Retrofit

TAG	Deficiency/unknown	Description
F2, F8	Insufficient shear walls	Provide new reinforced masonry shear walls in selected locations
F3	Insufficient footings.	Provide new or supplemental foundations.
R5	Inadequate out-of-plane connections between roof and masonry walls	Provide new out-of-plane connections and continuity ties to develop adequate sub diaphragms.
R6, R7	Inadequate drag ties at roof diaphragm	Provide new drag members and connections.
R8	Inadequate connections between metal deck and steel framing at roof	Provide additional welding of metal deck to the steel framing (this will require removing and replacing the roofing)

## 7.4 Building Part D Structural Seismic Retrofit

TAG	Deficiency/unknown	Description
F6	Insufficient anchor bolts at portal frame legs	Add supplemental bolts.
F7	Insufficient strength at portal frame moment connections	Add supplemental welded plates.



#	Deficiency/unknown	Description
N2	Masonry walls in locker room	Provide bracing
N3	Fire Suppression piping	Provide bracing
N4	Lay-in tile ceilings (at mezzanine)	Provide bracing and edge clearance detailing
N5	Other interior walls and partitions	Provide bracing
N6	Tall Narrow Contents	Provide bracing
N7	Fall-prone Contents over 20 lbs	Provide restraint
N8	Fall-prone Equipment over 20 lbs	Provide restraint
N9	Tall Narrow Equipment over 6 ft high	Provide bracing
N10	In-Line Equipment over 75 lb	Provide bracing
N11	Conduit Couplings	Provide flexible couplings
N12	Couplings for Fluid and Gas Pipe	Provide flexible couplings
N13	Gas shut-off valve	Provide automatic seismic shutoff valve
N14	Fluid and Gas Piping	Provide bracing
N15	Ducts Larger than 6 sf of Cross-Section	Provide bracing

## 7.5 Building Part A Nonstructural Seismic Retrofit

## 7.6 Building Part B Nonstructural Seismic Deficiencies

TAG	Deficiency/unknown	Description
N3	Fire Suppression piping	Provide bracing
N4	Lay-in tile ceilings	Provide bracing and edge clearance detailing
N5	Other interior walls and partitions	Provide bracing
N6	Tall Narrow Contents	Provide bracing
N7	Fall-prone Contents over 20 lbs	Provide restraint
N8	Fall-prone Equipment over 20 lbs	Provide restraint
N9	Tall Narrow Equipment over 6 ft high	Provide bracing
N10	In-Line Equipment over 75 lb	Provide bracing
N11	Conduit Couplings	Provide flexible couplings
N12	Couplings for Fluid and Gas Pipe	Provide flexible couplings
N13	Gas shut-off valve	Provide automatic seismic shutoff valve
N14	Fluid and Gas Piping	Provide bracing
N15	Ducts Larger than 6 sf of Cross-Section	Provide bracing



TAG	Deficiency/unknown	Description
N1	Brick pilasters at corridors	Provide bracing
N3	Fire Suppression piping	Provide bracing
N5	Other interior walls and partitions	Provide bracing
N6	Tall Narrow Contents	Provide bracing
N7	Fall-prone Contents over 20 lbs	Provide restraint
N8	Fall-prone Equipment over 20 lbs	Provide restraint
N9	Tall Narrow Equipment over 6 ft high	Provide bracing
N10	In-Line Equipment over 75 lb	Provide bracing
N14	Fluid and Gas Piping	Provide bracing
N15	Ducts Larger than 6 sf of Cross- Section	Provide bracing

## 7.7 Building Part C Nonstructural Seismic Deficiencies

## 7.8 Building Part D Nonstructural Seismic Deficiencies

No nonstructural retrofit measures are required.



## 8 SUMMARY CONSTRUCTION COST ESTIMATE

### 8.1 Direct Cost and Indirect Soft Cost

Direct Co	st	
Construction COW	\$	8,460,338
Sub total	\$	8,460,338
Indirect Soft	Cost	
Engineering	\$	1,100,000
Construction Management	\$	100,000
Relocation	\$	50,000
Construction Contingency	\$	1,300,000
Sub total	\$	2,550,000
Totals and Sur	nmary	
Total Cost Estimate	\$	11,010,338
Match Funds	\$	8,510,338
Total Amount Requested from SRGP	\$	2,500,000

\*Costs above are for Summer 2023 construction. An additional \$425,000 is estimated to be in addition to the construction costs above if delayed to Summer of 2024.

## 9 **RECOMMENDATIONS**

Based on the ASCE 41-17 Tier 1 screening, Five Oaks Middle School does not meet the performance objective and has a potential for partial collapse of the building particularly due to building Parts A, B and C having insufficient out-of-plane roof-to-wall connections, and Parts B and C having insufficient masonry shear walls.

### 10 CERTIFICATION STATEMENT

Holmes Structures reviewed the engineering cost estimate and certifies that all of the seismic deficiencies are included in the retrofit scope of work and that all of the retrofit's scope of work elements are included in the cost estimate.

Jennifer Eggers, S.E.

April 20, 2022





# **ASCE41-17 Tier 1 Checklists**

Project No. 21603.10



Page 20

	Project:	Five Oaks Middle School - Part A	
	Project No:	U21603.10	
nes	Completed By:	Mark Ellis	
	Reviewed By:	Jennifer Eggers	

Table 17-3: Immediate Occupancy Basic Configuration Checklist

#### Very Low Seismicity

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#### Building System - General

RATING			EVALUATION STATEMENT	COMMENTS	
С	NC	N/A	U	LOAD PATH: The structure contains a complete, well- defined load path, including structural elements and connections, that serves to transfer the inertial forces associated with the mass of all elements of the building to the foundation.	Tilt-up walls are not conneccted to foundations
С	NC	N/A	U	ADJACENT BUILDINGS: The clear distance between the building being evaluated and any adjacent building is greater than 0.5% of the height of the shorter building in low seismicity, 1.0% in moderate seismicity, and 3.0% in high seismicity.	1" expansion joint between Parts A and B is inadequate
С	NC	N/A	U	MEZZANINES: Interior mezzanine levels are braced independently from the main structure or are anchored to the seismic-force-resisting elements of the main structure.	
Buildi	ng Sy	stem - I	Build	ing Configuration	
RATI	NG			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	WEAK STORY: The sum of the shear strengths of the seismic-force-resisting system in any story in each direction is not less than 80% of the strength in the adjacent story above.	Single story building
С	NC	N/A	U	SOFT STORY: The stiffness of the seismic-force- resisting system in any story is not less than 70% of the seismic-force-resisting system stiffness in an adjacent story above or less than 80% of the average seismic- force-resisting system stiffness of the three stories above.	Single story building
С	NC	N/A	U	VERTICAL IRREGULARITIES: All vertical elements in the seismic-force-resisting system are continuous to the foundation.	Single story building
С	NC	N/A	U	GEOMETRY: There are no changes in the net horizontal dimension of the seismic-force-resisting system of more than 30% in a story relative to adjacent stories, excluding one-story penthouses and mezzanines.	Single story building
С	NC	N/A	U	MASS: There is no change in effective mass of more than 50% from one story to the next. Light roofs, penthouses, and mezzanines need not be considered.	Single story building
С	NC	N/A	U	TORSION: The estimated distance between the story center of mass and the story center of rigidity is less than 20% of the building width in either plan dimension.	

	Project:	Five Oaks Middle School - Part A
	Project No:	U21603.10
nes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-3: Immediate Occupancy Basic Configuration Checklist

#### Low Seismicity

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#### Geologic Site Hazards

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	LIQUEFACTION: Liquefaction-susceptible, saturated, loose granular soils that could jeopardize the building's seismic performance do not exist in the foundation soils at depths within 50 ft (15.2 m) under the building.	Site-specific geotechnical report for 2019 additions determined low liquefaction risk at site.
С	NC	N/A	U	SLOPE FAILURE: The building site is located away from potential earthquake- induced slope failures or rockfalls so that it is unaffected by such failures or is capable of accommodating any predicted movements without failure.	Site-specific geotechnical report for 2019 additions determined low landslide risk at site.
С	NC	N/A	U	SURFACE FAULT RUPTURE: Surface fault rupture and surface displacement at the building site are not anticipated.	

#### Moderate and High Seismicity

#### Foundation Configuration

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	OVERTURNING: The ratio of the least horizontal dimension of the seismic-force- resisting system at the foundation level to the building height (base/height) is greater than 0.6Sa.	
С	NC	N/A	U	TIES BETWEEN FOUNDATION ELEMENTS: The foundation has ties adequate to resist seismic forces where footings, piles, and piers are not restrained by beams, slabs, or soils classified as Site Class A, B, or C.	Strip footings at tilt-up walls are continuous

	Project:	Five Oaks Middle School - Part B
	Project No:	U21603.10
mes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-3: Immediate Occupancy Basic Configuration Checklist

#### Very Low Seismicity

Hol

#### Building System - General

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	LOAD PATH: The structure contains a complete, well- defined load path, including structural elements and connections, that serves to transfer the inertial forces associated with the mass of all elements of the building to the foundation.	
С	NC	N/A	U	ADJACENT BUILDINGS: The clear distance between the building being evaluated and any adjacent building is greater than 0.5% of the height of the shorter building in low seismicity, 1.0% in moderate seismicity, and 3.0% in high seismicity.	1" expansion joint between Parts A and B is inadequate
С	NC	N/A	U	MEZZANINES: Interior mezzanine levels are braced independently from the main structure or are anchored to the seismic-force-resisting elements of the main structure.	
Buildi	ng Sy	stem - I	Build	ing Configuration	
RATI	NG			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	WEAK STORY: The sum of the shear strengths of the seismic-force-resisting system in any story in each direction is not less than 80% of the strength in the adjacent story above.	Single story building
С	NC	N/A	U	SOFT STORY: The stiffness of the seismic-force- resisting system in any story is not less than 70% of the seismic-force-resisting system stiffness in an adjacent story above or less than 80% of the average seismic- force-resisting system stiffness of the three stories above.	Single story building
С	NC	N/A	U	VERTICAL IRREGULARITIES: All vertical elements in the seismic-force-resisting system are continuous to the foundation.	
С	NC	N/A	U	GEOMETRY: There are no changes in the net horizontal dimension of the seismic-force-resisting system of more than 30% in a story relative to adjacent stories, excluding one-story penthouses and mezzanines.	Single story building
С	NC	N/A	U	MASS: There is no change in effective mass of more than 50% from one story to the next. Light roofs, penthouses, and mezzanines need not be considered.	Single story building
С	NC	N/A	U	TORSION: The estimated distance between the story center of mass and the story center of rigidity is less than 20% of the building width in either plan dimension.	

	Project:	Five Oaks Middle School - Part B	
	Project No:	U21603.10	
nes	Completed By:	Mark Ellis	
	Reviewed By:	Jennifer Eggers	

Table 17-3: Immediate Occupancy Basic Configuration Checklist

#### Low Seismicity

Holr

#### Geologic Site Hazards

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	LIQUEFACTION: Liquefaction-susceptible, saturated, loose granular soils that could jeopardize the building's seismic performance do not exist in the foundation soils at depths within 50 ft (15.2 m) under the building.	Site-specific geotechnical report for 2019 additions determined low liquefaction risk at site.
С	NC	N/A	U	SLOPE FAILURE: The building site is located away from potential earthquake- induced slope failures or rockfalls so that it is unaffected by such failures or is capable of accommodating any predicted movements without failure.	Site-specific geotechnical report for 2019 additions determined low landslide risk at site.
С	NC	N/A	U	SURFACE FAULT RUPTURE: Surface fault rupture and surface displacement at the building site are not anticipated.	

#### Moderate and High Seismicity

#### Foundation Configuration

RATING				EVALUATION STATEMENT	COMMENTS
С	NC N/A U OVERTURNING: The ratio of the least horizontal dimension of the seismic-force- resisting system at the foundation level to the building height (base/height) is greater than 0.6Sa.		OVERTURNING: The ratio of the least horizontal dimension of the seismic-force- resisting system at the foundation level to the building height (base/height) is greater than 0.6Sa.		
С	NC	N/A	U	TIES BETWEEN FOUNDATION ELEMENTS: The foundation has ties adequate to resist seismic forces where footings, piles, and piers are not restrained by beams, slabs, or soils classified as Site Class A, B, or C.	Strip footings at perimter and interior shear walls are generally continuous

	Project:	Five Oaks Middle School - Part C
	Project No:	U21603.10
mes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-2: Collapse Prevention Basic Configuration Checklist

#### Low Seismicity

Ho

#### Building System - General

RATI	NG			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	LOAD PATH: The structure contains a complete, well- defined load path, including structural elements and connections, that serves to transfer the inertial forces associated with the mass of all elements of the building to the foundation.	
С	NC	N/A	U	ADJACENT BUILDINGS: The clear distance between the building being evaluated and any adjacent building is greater than 0.25% of the height of the shorter building in low seismicity, 0.5% in moderate seismicity, and 1.5% in high seismicity.	1" expansion joint between Parts A and B is inadequate. However the diaphragms are generally at the same elevation.
С	NC	N/A	U	MEZZANINES: Interior mezzanine levels are braced independently from the main structure or are anchored to the seismic-force-resisting elements of the main structure.	

Building System - Building Configuration

RATI	NG			EVALUATION STATEMENT	COMMENTS	
С	NC	N/A	U	WEAK STORY: The sum of the shear strengths of the seismic-force-resisting system in any story in each direction is not less than 80% of the strength in the adjacent story above.	Single story building	
С	NC	N/A	U	SOFT STORY: The stiffness of the seismic-force- resisting system in any story is not less than 70% of the seismic-force-resisting system stiffness in an adjacent story above or less than 80% of the average seismic- force-resisting system stiffness of the three stories above.	Single story building	
С	NC	N/A	U	VERTICAL IRREGULARITIES: All vertical elements in the seismic-force-resisting system are continuous to the foundation.		
С	NC	N/A	U	GEOMETRY: There are no changes in the net horizontal dimension of the seismic-force-resisting system of more than 30% in a story relative to adjacent stories, excluding one-story penthouses and mezzanines.	Single story building	
С	NC	N/A	U	MASS: There is no change in effective mass of more than 50% from one story to the next. Light roofs, penthouses, and mezzanines need not be considered.	Single story building	
С	NC	N/A	U	TORSION: The estimated distance between the story center of mass and the story center of rigidity is less than 20% of the building width in either plan dimension.		

	Project:	Five Oaks Middle School - Part C	
Project: Project No: Completed By Reviewed By:	Project No:	U21603.10	
olmes	Completed By:	Mark Ellis	
	Reviewed By:	Jennifer Eggers	

Table 17-2: Collapse Prevention Basic Configuration Checklist

#### Moderate Seismicity (Complete the Following Items in Addition to the Items for Low Seismicity)

#### Geologic Site Hazards

H

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	LIQUEFACTION: Liquefaction-susceptible, saturated, loose granular soils that could jeopardize the building's seismic performance do not exist in the foundation soils at depths within 50 ft (15.2 m) under the building.	Site-specific geotechnical report for 2019 additions determined low liquefaction risk at site.
С	NC	N/A	U	SLOPE FAILURE: The building site is located away from potential earthquake- induced slope failures or rockfalls so that it is unaffected by such failures or is capable of accommodating any predicted movements without failure.	Site-specific geotechnical report for 2019 additions determined low landslide risk at site.
С	NC	N/A	U	SURFACE FAULT RUPTURE: Surface fault rupture and surface displacement at the building site are not anticipated.	

High Seismicity (Complete the Following Items in Addition to the Items for Low and Moderate Seismicity)

#### Foundation Configuration

RATING				EVALUATION STATEMENT	COMMENTS
С	NC N/A U OVERTURNING: The ratio of the least horizontal dimension of the seismic-force- resisting system at the foundation level to the building height (base/height) is greater than 0.6Sa.		OVERTURNING: The ratio of the least horizontal dimension of the seismic-force- resisting system at the foundation level to the building height (base/height) is greater than 0.6Sa.		
С	NC	N/A	U	TIES BETWEEN FOUNDATION ELEMENTS: The foundation has ties adequate to resist seismic forces where footings, piles, and piers are not restrained by beams, slabs, or soils classified as Site Class A, B, or C.	Strip footings at perimter and interior shear walls are generally continuous

	Project:	Five Oaks Middle School - Part D
	Project No:	U21603.10
mes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-2: Collapse Prevention Basic Configuration Checklist

#### Low Seismicity

Ho

#### Building System - General

RATIN	NG			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	LOAD PATH: The structure contains a complete, well- defined load path, including structural elements and connections, that serves to transfer the inertial forces associated with the mass of all elements of the building to the foundation.	
С	NC	N/A	U	ADJACENT BUILDINGS: The clear distance between the building being evaluated and any adjacent building is greater than 0.25% of the height of the shorter building in low seismicity, 0.5% in moderate seismicity, and 1.5% in high seismicity.	2" separation is provided between Part D and Part A. This does not meet the 1.5% requirement, however the impacts of pounding are expected to be relatively minor, due to the lightweight nature of the Part D structure.
С	NC	N/A	U	MEZZANINES: Interior mezzanine levels are braced independently from the main structure or are anchored to the seismic-force-resisting elements of the main structure.	

Building System - Building Configuration

2 anui	Janonig Oysteni - Danonig Gonigunation						
RATING				EVALUATION STATEMENT	COMMENTS		
С	NC	N/A	U	WEAK STORY: The sum of the shear strengths of the seismic-force-resisting system in any story in each direction is not less than 80% of the strength in the adjacent story above.	Single story building		
С	NC	N/A	U	SOFT STORY: The stiffness of the seismic-force- resisting system in any story is not less than 70% of the seismic-force-resisting system stiffness in an adjacent story above or less than 80% of the average seismic- force-resisting system stiffness of the three stories above.	Single story building		
С	NC	N/A	U	VERTICAL IRREGULARITIES: All vertical elements in the seismic-force-resisting system are continuous to the foundation.			
С	NC	N/A	U	GEOMETRY: There are no changes in the net horizontal dimension of the seismic-force-resisting system of more than 30% in a story relative to adjacent stories, excluding one-story penthouses and mezzanines.	Single story building		
С	NC	N/A	U	MASS: There is no change in effective mass of more than 50% from one story to the next. Light roofs, penthouses, and mezzanines need not be considered.	Single story building		
С	NC	N/A	U	TORSION: The estimated distance between the story center of mass and the story center of rigidity is less than 20% of the building width in either plan dimension.			

	Project:	Five Oaks Middle School - Part D
	Project No:	U21603.10
olmes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-2: Collapse Prevention Basic Configuration Checklist

#### Moderate Seismicity (Complete the Following Items in Addition to the Items for Low Seismicity)

#### Geologic Site Hazards

H

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	LIQUEFACTION: Liquefaction-susceptible, saturated, loose granular soils that could jeopardize the building's seismic performance do not exist in the foundation soils at depths within 50 ft (15.2 m) under the building.	Site-specific geotechnical report for 2019 additions determined low liquefaction risk at site.
С	NC	N/A	U	SLOPE FAILURE: The building site is located away from potential earthquake- induced slope failures or rockfalls so that it is unaffected by such failures or is capable of accommodating any predicted movements without failure.	Site-specific geotechnical report for 2019 additions determined low landslide risk at site.
С	NC	N/A	U	SURFACE FAULT RUPTURE: Surface fault rupture and surface displacement at the building site are not anticipated.	

High Seismicity (Complete the Following Items in Addition to the Items for Low and Moderate Seismicity)

#### Foundation Configuration

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	OVERTURNING: The ratio of the least horizontal dimension of the seismic-force- resisting system at the foundation level to the building height (base/height) is greater than 0.6Sa.	
С	NC	N/A	U	TIES BETWEEN FOUNDATION ELEMENTS: The foundation has ties adequate to resist seismic forces where footings, piles, and piers are not restrained by beams, slabs, or soils classified as Site Class A, B, or C.	Foundation system is unknown, however foundation ties are not considered an important feature for this building.

	Project:	Five Oaks Middle School - Part A
	Project No:	U21603.10
es	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-29 - Immediate Occupancy Structural Checklist for Building Type PC1 and PC1a

#### Very Low Seismicity

Holm

Seismic-Force-Resisting System

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	REDUNDANCY: The number of lines of shear walls in each principal direction is greater than or equal to 2.	
С	NC	N/A	U	WALL SHEAR STRESS CHECK: The shear stress in the precast panels, calculated using the Quick Check procedure of Section 4.4.3.3., is less than the greater of 100lb/in <sup>2</sup> (0.69 MPa) or 2*sqrt(fc)	
С	NC	N/A	U	REINFORCING STEEL: The ratio of reinforcing steel area to gross concrete area is not less than 0.0012 in the vertical direction and 0.0020 in the horizontal direction. The speaing of the reinforcing steel is equal to or less than 18 in. (457 mm)	

Diaphragms (Stiff or Flexible)

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	TOPPING SLAB: Precast concrete diaphragm elements are interconnected by a continuous reinforced concrete topping slab with a minimum thickness of 2 in. (51 mm).	
0					

### Connections

RATIN	RATING			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	WALL ANCHORAGE: Exterior concrete or masonry walls that are dependent on the diaphragm for lateral support are anchored for out-of-plane forces at each diaphragm level with steel anchors, reinforcing dowels, or straps that are developed into the diaphragm. Connections have strength to resist the connection force calculated in the Quick Check procedure of Section 4.4.3.7.	In direction perpendicular to roof truss joists, joists are not welded to bearing plates in gym end walls (wall anchorage relies on ledger angle and metal deck, which is inadequate). In direction parallel to roof truss joists, no out-of-plane connections are provided at gym side walls (wall anchorage relies on ledger angle and metal deck, which is inadequate).
С	NC	N/A	U	WOOD LEDGERS: The connection between the wall panels and the diaphragm does not induce cross-grain bending or tension in the wood ledgers.	
С	NC	N/A	U	TRANSFER TO SHEAR WALLS: Diaphragms are connected for transfer of seismic forces to the shear walls, and the connections are able to develop the lesser of the shear strength or the walls or diaphragms.	Existing connections may not be able to develop the strength of the dipahragm after it is strengthened with new bracing.
С	NC	N/A	U	TOPPING SLAB TO WALLS OR FRAMES: Reinforced concrete topping slabs that interconnect the precast concrete diaphragm elements are doweled for transfer of forces into the shear wall or frame elements, and the dowels are able to develop the least of the shear strength of the walls, frames, or slabs.	
С	NC	N/A	U	GIRDER–COLUMN CONNECTION: There is a positive connection using plates, connection hardware, or straps between the girder and the column support.	There are no girders, however comments above re Wall Anchorage apply at pilasters also.
Found	ation	System	s		
RATIN	NG			EVALUATION STATEMENT	COMMENTS

				Project:	Five Oaks Middle School - Part A
				Project No:	U21603.10
н	olr	nes		Completed By:	Mark Ellis
	<b>U</b>	100		Reviewed By:	Jennifer Eggers
Tab	ole 17	7-29 -	Imr	nediate Occupancy Structural Checklis	st for Building Type PC1 and PC1a
С	NC	N/A	U	DEEP FOUNDATIONS: Piles and piers are capable of transferring the lateral forces between the structure and the soil.	
С	NC	N/A	U	SLOPING SITES: The difference in foundation embedment depth from one side of the building to another does not exceed one story.	
Low,	Mode	rate and	d Hig	h Seismicity (Complete the Following Items in Addition	n to the Items for Very Low Seismicity)
Seisn	nic-Fo	orce-Kes	sisting		CO10(EX/70
KAL	ING		r	EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	DIAPHRAGMS: Secondary components have the shear capacity to develop the flexural strength of the components.	
С	NC	N/A	U	WALL OPENINGS: The total width of openings along any perimeter wall line constitutes less than 50% of the length of any perimeter wall when the wall piers have aspect ratios of less than 2-to-1.	
С	NC	N/A	U	PANEL-TO-PANEL CONNECTIONS: Adjacent wall panels are interconnected to transfer overturning forces between panels by nethods other than welded steel inserts.	Horzontall bars in panels are embedded into the insitu pilasters.
С	NC	N/A	U	WALL THICKNESS: Thicknesses of bearing walls are not less than 1/25 the unsupported height or length, whichever is shorter, nor less than 4 in. (101 mm).	Walls span horizontally up to 16 ft between pilasters (15 ft clear span). 15 ft / $25 = 7.2$ inches, whereas panel thickness is 6 inches. However we assume that this will be determined by Tier 2 analysis to be ok.
Diap	hragn	ıs		•	
RAT	ING			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	CROSS TIES IN FLEXIBLE DIAPHRAGMS: There are continuous cross ties between diaphragm chords.	No cross ties are provided in direction perpendicular to roof truss joists.
С	NC	N/A	U	PLAN IRREGULARITIES: There is tensile capacity to develop the strength of the diaphragm at reentrant corners or other locations of plan irregularities.	
С	NC	N/A	U	PIAGHRAGM REINFORCEMENT AT OPENINGS: There is reinforcing around all diaphragm openings larger than 50% of the building width in either major plan dimension.	
С	NC	N/A	U	STRAIGHT SHEATHING: All straight-sheathed diaphragms have aspect ratios less than 1-to-1 in the direction being considered.	
С	NC	N/A	U	SPANS: All wood diaphragms with spans greater than 12 ft (3.6 m) consist of wood structural panels or diagonal sheathing.	
С	NC	N/A	U	DIAGONALLY SHEATHED AND UNBLOCKED DIAPHRAGMS: All diagonally sheathed or unblocked wood structural panel diaphragms have horizontal spans less than 30 ft (9.2 m) and aspect ratios less than or equal to 3-to-1.	
С	NC	N/A	U	OTHER DIAPHRAGMS: Diaphragms do not consist of a system other than wood, metal deck, concrete, or horizontal bracing.	

	Project:	Five Oaks Middle School - Part A
	Project No:	U21603.10
Holmes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-29 - Immediate Occupancy Structural Checklist for Building Type PC1 and PC1a

Conne	Connections						
RATING				EVALUATION STATEMENT	COMMENTS		
С	NC	N/A	U	MINIMUM NUMBER OF WALL ANCHORS PER PANEL: There are at least two anchors connecting each precast wall panel to the diaphragm elements.	See Wall Anchorage comments above		
С	NC	N/A	U	PRECAST WALL PANELS: Precast wall panels are connected to the foundation, and the connections are able to develop the strength of the walls.	Wall panels are not connected to the foundations.		
С	NC	N/A	U	UPLIFT AT PILE CAPS: Pile caps have top reinforcement, and piles are anchored to the pile caps; the pile cap reinforcement and pile anchorage are able to develop the tensile capacity of the piles.			
С	NC	N/A	U	GIRDERS: Girders supported by walls or pilasters have at least two ties securing the anchor bolts unless provided with independent stiff wall anchors with strength to resist the connection force calculated in the Quick Check procedure of Section 4.4.3.7.	See Wall Anchorage comments above		

	Project:	Five Oaks Middle School - Part B
	Project No:	U21603.10
nes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-35 - Immediate Occupancy Structural Checklist for Building Type RM1

#### Very Low Seismicity

Holr

Seismic-Force-Resisting System

RATI	NG			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	REDUNDANCY: The number of lines of shear walls in each principal direction is greater than or equal to 2.	
С	NC	N/A	U	SHEAR STRESS CHECK: The shear stress in the reinforced masonry shear walls, calculated using the Quick Check procedure of Section 4.4.3.3, is less than 70 lb/in <sup>2</sup> (4.83 MPa).	Some walls are non-compliant
С	NC	N/A	U	REINFORCING STEEL: The total vertical and horizontal reinforcing steel ratio in reinforced masonry walls is greater than 0.002 of the wall with the minimum of 0.0007 in either of the two directions; the spacing of reinforcing steel is less than 48 in., and all vertical bars extend to the top of the walls.	

Connections

RATI	RATING EVALUATION STATEMENT COMMENTS						
С	NC	N/A	U	WALL ANCHORAGE: Exterior concrete or masonry walls that are dependent on the diaphragm for lateral support are anchored for out-of-plane forces at each diaphragm level with steel anchors, reinforcing dowels, or straps that are developed into the diaphragm. Connections have strength to resist the connection force calculated in the Quick Check procedure of Section 4.4.3.7.	In direction perpendicular to roof truss joists, joists are welded to bearing plates in walls and these connections comply with the quick check. However in direction parallel to roof truss joists, no out-of- plane connections are provided at walls (wall anchorage relies on metal deck, which is not acceptable).		
С	NC	N/A	U	WOOD LEDGERS: The connection between the wall panels and the diaphragm does not induce cross-grain bending or tension in the wood ledgers.			
С	NC	N/A	U	TRANSFER TO SHEAR WALLS: Diaphragms are connected for transfer of seismic forces to the shear walls, and the connections are able to develop the lesser of the shear strength of the walls or diaphragms.			
С	NC	N/A	U	FOUNDATION DOWELS: Wall reinforcement is doweled into the foundation, and the dowels are able to develop the lesser of the strength of the walls or the uplift capacity of the foundation.			
С	NC	N/A	U	GIRDER–COLUMN CONNECTION: There is a positive connection using plates, connection hardware, or straps between the girder and the column support.			

	Project:	Five Oaks Middle School - Part B
	Project No:	U21603.10
lolmes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-35 - Immediate Occupancy Structural Checklist for Building Type RM1

#### Stiff Diaphragms

ŀ

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	TOPPING SLAB: Precast concrete diaphragm elements are interconnected by a continuous reinforced concrete topping slab.	
С	NC	N/A	U	TOPPING SLAB TO WALLS OR FRAMES: Reinforced concrete topping slabs that interconnect the precast concrete diaphragm elements are doweled for transfer of forces into the shear wall or frame elements.	

#### Foundation Systems

1 oundation bystems						
RATING			EVALUATION STATEMENT	COMMENTS		
NC	N/A	U	DEEP FOUNDATIONS: Piles and piers are capable of transferring the lateral forces between the structure and the soil.			
NC	N/A	U	SLOPING SITES: The difference in foundation embedment depth from one side of the building to another does not exceed one story.			
	NG NC NC	NC N/A	NC N/A U NC N/A U	NG EVALUATION STATEMENT   NC N/A U   DEEP FOUNDATIONS: Piles and piers are capable of transferring the lateral forces between the structure and the soil.   NC N/A U   SLOPING SITES: The difference in foundation embedment depth from one side of the building to another does not exceed one story.		

## Low, Moderate, and High Seismicity

#### Seismic-Force-Resisting System

			0		
RATING				EVALUATION STATEMENT	COMMENTS
				REINFORCING AT WALL OPENINGS: All wall	
С	NC	N/A	U	openings that interrupt rebar have trim reinforcing on	
				all sides.	
C	NC	NT / A	TT	PROPORTIONS: The height-to-thickness ratio of the	
C	NC	N/A	U	shear walls at each story is less than 30.	

#### Diaphragms (Stiff or Flexible)

RATI	RATING			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	OPENINGS AT SHEAR WALLS: Diaphragm openings immediately adjacent to the shear walls are less than 15% of the wall length.	
С	NC	N/A	U	OPENINGS AT EXTERIOR MASONRY SHEAR WALLS: Diaphragm openings immediately adjacent to exterior masonry shear walls are not greater than 4 ft (1.2 m) long.	
С	NC	N/A	U	PLAN IRREGULARITIES: There is tensile capacity to develop the strength of the diaphragm at reentrant corners or other locations of plan irregularities.	
С	NC	N/A	U	DIAPHRAGM REINFORCEMENT AT OPENINGS: There is reinforcing around all diaphragm openings larger than 50% of the building width in either major plan dimension.	

	Project:	Five Oaks Middle School - Part B
	Project No:	U21603.10
Holmes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-35 - Immediate Occupancy Structural Checklist for Building Type RM1

#### Flexible Diaphragms

RATI	NG			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	CROSS TIES: There are continuous cross ties between diaphragm chords.	No cross ties are provided in direction perpendicular to roof truss joists.
С	NC	N/A	U	STRAIGHT SHEATHING: All straight-sheathed diaphragms have aspect ratios less than 1-to-1 in the direction being considered.	
С	NC	N/A	U	SPANS: All wood diaphragms with spans greater than 12 ft (3.6 m) consist of wood structural panels or diagonal sheathing.	
С	NC	N/A	U	DIAGONALLY SHEATHED AND UNBLOCKED DIAPHRAGMS: All diagonally sheathed or unblocked wood structural panel diaphragms have horizontal spans less than 30 ft (9.2 m) and aspect ratios less than or equal to 3-to-1	
С	NC	N/A	U	NONCONCRETE FILLED DIAPHRAGMS: Untopped metal deck diaphragms or metal deck diaphragms with fill other than concrete consist of horizontal spans of less than 40 ft (12.2 m) and have aspect ratios less than 4-to-1.	Some areas of the metal deck diaphragm have spans greater than 40 ft.
С	NC	N/A	U	OTHER DIAPHRAGMS: Diaphragms do not consist of a system other than wood, metal deck, concrete, or horizontal bracing.	
Conne	ection	s			
RATI	NG			EVALUATION STATEMENT	COMMENTS

0011110	Competitions						
RATING				EVALUATION STATEMENT	COMMENTS		
С	NC	N/A	U	STIFFNESS OF WALL ANCHORS: Anchors of concrete or masonry walls to wood structural elements are installed taut and are stiff enough to limit the relative movement between the wall and the diaphragm to no greater than 1/8 in. before engagement of the anchors.	See Wall Anchorage comments above		

	Project:	Five Oaks Middle School - Part C
	Project No:	U21603.10
mes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

Table 17-34. Collapse Prevention Structural Checklist for Building Types RM1 and RM2

#### Low and Moderate Seismicity

Hol

#### Seismic-Force-Resisting System

RATI	NG			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	REDUNDANCY: The number of lines of shear walls in each principal direction is greater than or equal to 2.	
С	NC	N/A	U	SHEAR STRESS CHECK: The shear stress in the reinforced masonry shear walls, calculated using the Quick Check procedure of Section 4.4.3.3, is less than 70 lb/in.2 (0.48 MPa).	Some walls are non-compliant
С	NC	N/A	U	REINFORCING STEEL: The total vertical and horizontal reinforcing steel ratio in reinforced masonry walls is greater than 0.002 of the wall with the minimum of 0.0007 in either of the two directions; the spacing of reinforcing steel is less than 48 in. (1220 mm), and all vertical bars extend to the top of the walls.	

#### Stiff Diaphragms

	-	0			
RATING				EVALUATION STATEMENT	COMMENTS
				TOPPING SLAB: Precast concrete diaphragm elements	
С	NC	N/A	U	are interconnected by a continuous reinforced concrete	
				topping slab.	

Connections

RATING				EVALUATION STATEMENT	COMMENTS				
С	NC	N/A	U	WALL ANCHORAGE: Exterior concrete or masonry walls that are dependent on the diaphragm for lateral support are anchored for out-of-plane forces at each diaphragm level with steel anchors, reinforcing dowels, or straps that are developed into the diaphragm. Connections have strength to resist the connection force calculated in the Quick Check procedure of Section 4.4.3.7.	In direction perpendicular to roof truss joists, joists are welded to bearing plates in walls and these connections comply with the quick check. However in direction parallel to roof truss joists, no out-of- plane connections are provided at walls (wall anchorage relies on metal deck, which is not acceptable).				
С	NC	N/A	U	WOOD LEDGERS: The connection between the wall panels and the diaphragm does not induce cross-grain bending or tension in the wood ledgers.					
С	NC	N/A	U	TRANSFER TO SHEAR WALLS: Diaphragms are connected for transfer of seismic forces to the shear walls.					
С	NC	N/A	U	TOPPING SLAB TO WALLS OR FRAMES: Reinforced concrete topping slabs that interconnect the precast concrete diaphragm elements are doweled for transfer of forces into the shear wall or frame elements.					
С	NC	N/A	U	FOUNDATION DOWELS: Wall reinforcement is doweled into the foundation.					
С	NC	N/A	U	GIRDER–COLUMN CONNECTION: There is a positive connection using plates, connection hardware, or straps between the girder and the column support.					
	Project:	Five Oaks Middle School - Part C							
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	Project No:	U21603.10							
olmes	Completed By:	Mark Ellis							
	Reviewed By:	Jennifer Eggers							

Table 17-34. Collapse Prevention Structural Checklist for Building Types RM1 and RM2

High Seismicity (Complete the Following Items in Addition to the Items for Low and Moderate Seismicity) *Stiff Diaphragms* 

RATING				EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	OPENINGS AT SHEAR WALLS: Diaphragm openings immediately adjacent to the shear walls are less than 25% of the wall length.	
С	NC	N/A	U	OPENINGS AT EXTERIOR MASONRY SHEAR WALLS: Diaphragm openings immediately adjacent to exterior masonry shear walls are not greater than 8 ft (2.4 m) long.	

Flexible Diaphragms

H

RATI	NG	-pining		EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	CROSS TIES: There are continuous cross ties between diaphragm chords.	No cross ties are provided in direction perpendicular to roof truss joists.
С	NC	N/A	U	OPENINGS AT SHEAR WALLS: Diaphragm openings immediately adjacent to the shear walls are less than 25% of the wall length.	
С	NC	N/A	U	OPENINGS AT EXTERIOR MASONRY SHEAR WALLS: Diaphragm openings	
С	NC	N/A	U	STRAIGHT SHEATHING: All straight-sheathed diaphragms have aspect ratios less than 2-to-1 in the direction being considered.	
С	NC	N/A	U	SPANS: All wood diaphragms with spans greater than 24 ft (7.3 m) consist of wood structural panels or	
С	NC	N/A	U	DIAGONALLY SHEATHED AND UNBLOCKED DIAPHRAGMS: All diagonally sheathed or unblocked wood structural panel diaphragms have horizontal spans less than 40 ft (12.2 m) and aspect ratios less than or equal to 4-to-1.	
С	NC	N/A	U	OTHER DIAPHRAGMS: Diaphragms do not consist of a system other than wood, metal deck, concrete, or horizontal bracing.	
Conne	ection	ıs			
RATI	NG			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	STIFFNESS OF WALL ANCHORS: Anchors of concrete or masonry walls to wood structural elements are installed taut and are stiff enough to limit the relative movement between the wall and the diaphragm to no greater than 1/8 in. (3 mm) before engagement of the anchors.	See Wall Anchorage comments above

	Project:	Five Oaks Middle School - Part D
	Project No:	U21603.10
Holmes	Completed By:	Mark Ellis
	Reviewed By:	Jennifer Eggers

 Table 17-12. Collapse Prevention Structural Checklist for Building Type S3

#### Low and Moderate Seismicity

#### Seismic-Force-Resisting System

RATING EVALUATION STATEMENT				EVALUATION STATEMENT	COMMENTS	
С	C NC N/A U		U	BRACE AXIAL STRESS CHECK: The axial stress in the diagonals, calculated using the Quick Check procedure of Section 4.4.3.4, is less than 0.50Fy.	Moment Frames in both directions	
Conne	Connections					
RATI	RATING			EVALUATION STATEMENT	COMMENTS	
С	NC	N/A	U	TRANSFER TO STEEL FRAMES: Diaphragms are connected for transfer of seismic forces to the steel moment frames.	No structural drawings are available, however this is not expected to be a significant concern.	
С	NC	N/A	U	STEEL COLUMNS: The columns in seismic-force- resisting frames are anchored to the building foundation	Bolts do not appear adequate	

High Seismicity (Complete the Following Items in Addition to the Items for Low and Moderate Seismicity)

#### Seismic-Force-Resisting System

RATING				EVALUATION STATEMENT	COMMENTS
				MOMENT-RESISTING CONNECTIONS: All	Moment frame connections in portal frames along each side
С	NC	N/A	U	moment connections are able to develop the elastic	may not be adequate.
				moment (FyS) of the adjoining members.	
				COMPACT MEMBERS: All frame elements meet	No structural drawings are available, however this is not
С	NC	N/A	U	compact section requirements in accordance with AISC	expected to be a significant concern.
				360, Table B4.1.	

Diaphragms

RATING				EVALUATION STATEMENT	COMMENTS	
				OTHER DIAPHRAGMS: Diaphragms do not consist		
С	NC	N/A	U	of a system other than wood, metal deck, concrete, or		
				horizontal bracing.		
Conne	Connections					
RATIN	NG			EVALUATION STATEMENT	COMMENTS	
				ROOF PANELS: Where considered as diaphragm	No structural drawings are available, however this is not	

 C
 N/A
 U
 ROOF PANELS: Where considered as diaphragm elements for lateral resistance, metal, plastic, or cementitious roof panels are positively attached to the roof framing to resist seismic forces.
 No structural drawings are available, however this is not expected to be a significant concern.

 C
 NC
 N/A
 U
 WALL PANELS: Where considered as shear elements for lateral resistance, metal, fiberglass, or cementitious wall panels are positively attached to the framing and foundation to resist seismic forces.
 No structural drawings are available, however this is not expected to be a significant concern.

	Project:	Five Oaks Middle School
	Project No:	21603.10
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noimes	Reviewed By:	Jennifer Eggers

Table 17-38 - Nonstructural Checklist

#### Life Safety Systems

STAT	US			EVALUATION STATEMENT	COMMENTS
C	NC	NI/A	TT	HR-not required; LS-LMH; PR-LMH. FIRE SUPPRESSION PIPING: Fire	
C	INC.	11/11	U	suppression piping is anchored and braced in accordance with NFPA-13.	
C	NC	NT/A	П	HR-not required; LS-LMH; PR-LMH. FLEXIBLE COUPLINGS: Fire suppression	
C	INC	$1N/\Lambda$	U	piping has flexible couplings in accordance with NFPA-13.	
C	NC	NI/A	П	HR-not required; LS-LMH; PR-LMH. EMERGENCY POWER: Equipment used	
C	INC.	11/11	U	to power or control Life Safety systems is anchored or braced.	
				HR—not required; LS—LMH; PR—LMH. STAIR AND SMOKE DUCTS: Stair	
С	NC	N/A	U	pressurization and smoke control ducts are braced and have flexible connections at	
				seismic joints.	
				HR-not required; LSMH; PR-MH. SPRINKLER CEILING CLEARANCE:	
С	NC	N/A	U	Penetrations through panelized ceilings for fire suppression devices provide clearances in	
				accordance with NFPA-13.	
C	NC	NI/A	II	HR-not required; LS-not required; PR-LMH. EMERGENCY LIGHTING: Emergency	Needs to be verified
C	INC	$1N/\Lambda$	0	and egress lighting equipment is anchored or braced.	(Not required at Part C)

Hazardous Materials

STAT	US			EVALUATION STATEMENT	COMMENTS
				HR-LMH; LS-LMH; PR-LMH. HAZARDOUS MATERIAL EQUIPMENT:	Needs to be verified. Snap report notes
С	NC	N/A	U	Equipment mounted on vibration isolators and containing hazardous material is	"Presumed Postive" materials in various
				equipped with restraints or snubbers.	locations.
				HR-LMH; LS-LMH; PR-LMH. HAZARDOUS MATERIAL STORAGE: Breakable	Needs to be verified. Snap report notes
С	NC	N/A	U	containers that hold hazardous material, including gas cylinders, are restrained by latched	"Presumed Postive" materials in various
				doors, shelf lips, wires, or other methods.	locations.
				HR-MH; LS-MH; PR-MH. HAZARDOUS MATERIAL DISTRIBUTION: Piping or	Needs to be verified. Snap report notes
С	NC	N/A	U	ductwork conveying hazardous materials is braced or otherwise protected from damage	"Presumed Postive" materials in various
				that would allow hazardous material release.	locations.
				HR-MH; LS-MH; PR-MH. SHUTOFF VALVES: Piping containing hazardous material,	Needs to be verified. Snap report notes
С	NC	N/A	U	including natural gas, has shutoff valves or other devices to limit spills or leaks.	"Presumed Postive" materials in various
					locations.
				HR-LMH; LS-LMH; PR-LMH. FLEXIBLE COUPLINGS: Hazardous material	Needs to be verified. Snap report notes
С	NC	N/A	U	ductwork and piping, including natural gas piping, have flexible couplings.	"Presumed Postive" materials in various
					locations.
				HR-MH; LS-MH; PR-MH. PIPING OR DUCTS CROSSING SEISMIC JOINTS:	Needs to be verified. Snap report notes
C	NC	NI/A	п	Piping or ductwork carrying hazardous material that either crosses seismic joints or	"Presumed Postive" materials in various
C	C NC	1N/A	U	isolation planes or is connected to independent structures has couplings or other details	locations.
				to accommodate the relative seismic displacements.	

	Project:	Five Oaks Middle School
	Project No:	21603.10
	Completed By:	Mark Ellis
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Table 17-38 - Nonstructural Checklist

Partitions

STAT	US			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	HR—LMH; LS—LMH; PR—LMH. UNREINFORCED MASONRY: Unreinforced masonry or hollow-clay tile partitions are braced at a spacing of at most 10 ft (3.0 m) in Low or Moderate Seismicity, or at most 6 ft (1.8 m) in High Seismicity.	
С	NC	N/A	U	HR—LMH; LS—LMH; PR—LMH. HEAVY PARTITIONS SUPPORTED BY CEILINGS: The tops of masonry or hollow-clay tile partitions are not laterally supported by an integrated ceiling system.	Brick pilasters at Part C need bracing. Bracing for masonry walls at other areas need to be verified.
С	NC	N/A	U	HR—not required; LS—MH; PR—MH. DRIFT: Rigid cementitious partitions are detailed to accommodate the following drift ratios: in steel moment frame, concrete moment frame, and wood frame buildings, 0.02; in other buildings, 0.005.	Needs to be verified
С	NC	N/A	U	HR—not required; LS—not required; PR—MH. LIGHT PARTITIONS SUPPORTED BY CEILINGS: The tops of gypsum board partitions are not laterally supported by an integrated ceiling system.	Needs to be verified (Not required at Part C)
С	NC	N/A	U	HR—not required; LS—not required; PR—MH. STRUCTURAL SEPARATIONS: Partitions that cross structural separations have seismic or control joints.	Needs to be verified (Not required at Part C)
С	NC	N/A	U	HR—not required; LS—not required; PR—MH. TOPS: The tops of ceiling-high framed or panelized partitions have lateral bracing to the structure at a spacing equal to or less than 6 ft (1.8 m)	Needs to be verified (Not required at Part C)

Coilin							
Cenin							
STAT	US			EVALUATION STATEMENT	COMMENTS		
				HR-H; LS-MH; PR-LMH. SUSPENDED LATH AND PLASTER: Suspended lath			
С	NC	N/A	U	and plaster ceilings have attachments that resist seismic forces for every 12 ft2 (1.1 m2)			
				of area.			
				HR—not required; LS—MH; PR—LMH. SUSPENDED GYPSUM BOARD:	Needs to be verified		
С	NC	N/A	U	Suspended gypsum board ceilings have attachments that resist seismic forces for every 12			
				ft2 (1.1 m2) of area.			
				HR—not required: LS—not required: PR—MH. INTEGRATED CEILINGS:	Not required at Part C		
				Integrated suspended ceilings with continuous areas greater than 144 ft2 (13.4 m2) and	1		
				ceilings of smaller areas that are not surrounded by restraining partitions are laterally			
C	NC	N/A	П	restrained at a spacing no greater than 12 ft (3.6 m) with members attached to the			
C	110	1 1/ 11	0	estructure above. Each restraint location has a minimum of four diagonal wires and			
				compression strute, or diagonal members capable of registing compression			
				compression struts, or magonar members capable or resisting compression.			
				UP not required: US not required: DP MH EDCE CLEAPANCE: The free edges	Not required at Part C		
				a first and a siling with a siling structure of the state of the siling structure of the siling struct	Not required at Fart C		
0	210	NT / A	**	or integrated suspended ceilings with continuous areas greater than 144 ft2 (13.4 m2)			
C	NC	N/A	U	have clearances from the enclosing wall or partition of at least the following: in Moderate			
				Seismicity, $1/2$ in. (13 mm); in High Seismicity, $3/4$ in. (19 mm).			
_				HR—not required; LS—not required; PR—MH. CONTINUITY ACROSS	Assume non-compliant at joint between Part		
С	NC	N/A	U	STRUCTURE JOINTS: The ceiling system does not cross any seismic joint and is not	B and Part C.		
				attached to multiple independent structures.			
				HR—not required; LS—not required; PR—H. EDGE SUPPORT: The free edges of	Not required at Part C		
С	NC	N/A	U	integrated suspended ceilings with continuous areas greater than 144 ft2 (13.4 m2) are			
				supported by closure angles or channels not less than 2 in. (51 mm) wide.			
				HR-not required; LS-not required; PR-H. SEISMIC JOINTS: Acoustical tile or lay-	Not required at Part C		
C	NIC	NI/A	П	in panel ceilings have seismic separation joints such that each continuous portion of the			
C	INC	1N/11	U	ceiling is no more than 2,500 ft2 (232.3 m2) and has a ratio of long-to-short dimension			
				no more than 4-to-1.			

	Project:	Five Oaks Middle School
	Project No:	21603.10
	Completed By:	Mark Ellis
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#### Table 17-38 - Nonstructural Checklist

Light Fixtures

STAT	US			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	HR—not required; LS—MH; PR—MH. INDEPENDENT SUPPORT: Light fixtures that weigh more per square foot than the ceiling they penetrate are supported independent of the grid ceiling suspension system by a minimum of two wires at	
				diagonally opposite corners of each fixture.	
С	NC	N/A	U	HR—not required; LS—not required; PR—H. PENDANT SUPPORTS: Light fixtures on pendant supports are attached at a spacing equal to or less than 6 ft. Unbraced suspended fixtures are free to allow a 360-degree range of motion at an angle not less than 45 degrees from horizontal without contacting adjacent components. Alternatively, if rigidly supported and/or braced, they are free to move with the structure to which they are attached without damaging adjoining components. Additionally, the connection to the structure is capable of accommodating the movement without failure.	Needs to be verified (Not required at Part C)
С	NC	N/A	U	HR—not required; LS—not required; PR—H. LENS COVERS: Lens covers on light fixtures are attached with safety devices.	
Cladd	ing a	nd Glaz	zing		

STAT	US		0	EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	HR—MH; LS—MH; PR—MH. CLADDING ANCHORS: Cladding components weighing more than 10 lb/ft2 (0.48 kN/m2) are mechanically anchored to the structure at a spacing equal to or less than the following: for Life Safety in Moderate Seismicity, 6 ft (1.8 m); for Life Safety in High Seismicity and for Position Retention in any seismicity, 4 ft (1.2 m)	
С	NC	N/A	U	HR—not required; LS—MH; PR—MH. CLADDING ISOLATION: For steel or concrete moment-frame buildings, panel connections are detailed to accommodate a story drift ratio by the use of rods attached to framing with oversize holes or slotted holes of at least the following: for Life Safety in Moderate Seismicity, 0.01; for Life Safety in High Seismicity and for Position Retention in any seismicity, 0.02, and the rods have a length-to-diameter ratio of 4.0 or less.	
С	NC	N/A	U	HR—MH; LS—MH; PR—MH. MULTI-STORY PANELS: For multi-story panels attached at more than one floor level, panel connections are detailed to accommodate a story drift ratio by the use of rods attached to framing with oversize holes or slotted holes of at least the following: for Life Safety in Moderate Seismicity, 0.01; for Life Safety in High Seismicity and for Position Retention in any seismicity, 0.02, and the rods have a length-to-diameter ratio of 4.0 or less.	
С	NC	N/A	U	HR—not required; LS—MH; PR—MH. THREADED RODS: Threaded rods for panel connections detailed to accommodate drift by bending of the rod have a length-to- diameter ratio greater than 0.06 times the story height in inches for Life Safety in Moderate Seismicity and 0.12 times the story height in inches for Life Safety in High Seismicity and Position Retention in any seismicity.	
С	NC	N/A	U	HR—MH; LS—MH; PR—MH. PANEL CONNECTIONS: Cladding panels are anchored out of plane with a minimum number of connections for each wall panel, as follows: for Life Safety in Moderate Seismicity, 2 connections; for Life Safety in High Seismicity and for Position Retention in any seismicity, 4 connections.	
С	NC	N/A	U	HR—MH; LS—MH; PR—MH. BEARING CONNECTIONS: Where bearing connections are used, there is a minimum of two bearing connections for each cladding panel.	
С	NC	N/A	U	HR—MH; LS—MH; PR—MH. INSERTS: Where concrete cladding components use inserts, the inserts have positive anchorage or are anchored to reinforcing steel.	
С	NC	N/A	U	HR—not required; LS—MH; PR—MH. OVERHEAD GLAZING: Glazing panes of any size in curtain walls and individual interior or exterior panes more than 16 ft2 (1.5 m2) in area are laminated annealed or laminated heat-strengthened glass and are detailed to remain in the frame when cracked.	Needs to be verified at other areas with panes more than 16 ft2 in area

	Project:	Five Oaks Middle School
	Project No:	21603.10
	Completed By:	Mark Ellis
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#### Table 17-38 - Nonstructural Checklist

Masonry Veneer

С

NC N/A U

STAT	'US			EVALUATION STATEMENT	COMMENTS
				HR-not required; LS-LMH; PR-LMH. TIES: Masonry veneer is connected to the	
				backup with corrosion-resistant ties. There is a minimum of one tie for every 2-2/3 ft2	
С	NC	N/A	U	$(0.25 \text{ m}^2)$ , and the ties have spacing no greater than the following: for Life Safety in Low	
_				or Moderate Seismicity, 36 in. (914 mm); for Life Safety in High Seismicity and for	
				Position Retention in any seismicity. 24 in. (610 mm).	
				HR—not required: LS—LMH: PR—LMH_SHELF ANGLES: Masonry veneer is	
С	NC	N/A	U	supported by shelf angles or other elements at each floor above the ground floor	
				HR_not required I S_I MH: PR_I MH WEAKENED PI ANES: Masonry veneer	
C	NC	N/A	II	is anchored to the backup adjacent to weakened planes, such as at the locations of	
C	110	1 1/ 21	0	faching	
	-			HR IMHIS IMHIDR IMH UNREINEORCED MASONRY BACKUD. There	
С	NC	N/A	U	in a unsolver mesony hadron	
				LIP not required LS MIL DP MIL STUD TPACKS. For yoncor with gold formed	
C	NC	NI / A	TT	ated atud beginne atud tracks are featured to the structure at a specing actual to at less	
C	NC	$1N/\Lambda$	U	steel stud backup, stud tracks are fasteried to the structure at a spacing equal to or less	
				than 24 in. (610 mm) on center.	
				HR—not required; LS—MH; PR—MH. ANCHORAGE: For veneer with concrete	
С	NC	N/A	U	block or masonry backup, the backup is positively anchored to the structure at a	
				horizontal spacing equal to or less than 4 ft along the floors and root.	
С	NC	N/A	U	HR—not required; LS—not required; PR—MH. WEEP HOLES: In veneer anchored to	
		.,	_	stud walls, the veneer has functioning weep holes and base flashing.	
С	NC	N/A	U	HR—not required; LS—not required; PR—MH. OPENINGS: For veneer with cold-	
0			Ŭ	formed-steel stud backup, steel studs frame window and door openings.	
Parap	oets, C	Cornice	s, Or	namentations, and Appendages	
STAT	US			EVALUATION STATEMENT	COMMENTS
				HR—LMH; LS—LMH; PR—LMH. URM PARAPETS OR CORNICES: Laterally	
				unsupported unreinforced masonry parapets or cornices have height-to- thickness ratios	
С	NC	N/A	U	no greater than the following: for Life Safety in Low or Moderate Seismicity, 2.5; for Life	
				Safety in High Seismicity and for Position Retention in any seismicity, 1.5.	
				HR-not required; LS-LMH; PR-LMH. CANOPIES: Canopies at building exits are	
C	NC	NI / A	TT	anchored to the structure at a spacing no greater than the following: for Life Safety in	
C	NC	$1N/\Lambda$	U	Low or Moderate Seismicity, 10 ft (3.0 m); for Life Safety in High Seismicity and for	
				Position Retention in any seismicity, 6 ft (1.8 m).	
6	NC	NT / A	1.1	HR-H; LS-MH; PR-LMH. CONCRETE PARAPETS: Concrete parapets with	
C	NC	N/A	U	height-to-thickness ratios greater than 2.5 have vertical reinforcement.	
				HR-MH; LS-MH; PR-LMH. APPENDAGES: Cornices, parapets, signs, and other	
				ornamentation or appendages that extend above the highest point of anchorage to the	
				structure or cantilever from components are reinforced and anchored to the structural	
С	NC	N/A	U	system at a spacing equal to or less than 6 ft $(1.8 \text{ m})$ . This evaluation statement item does	
				not apply to parapets or cornices covered by other evaluation statements.	
Maso	nrv C	himnes	75	1	
STAT	US _		-	EVALUATION STATEMENT	COMMENTS
				HR—LMH: LS—LMH: PR—LMH_URM CHIMNEYS: Unreinforced masonry	
1				chimneys extend above the roof surface no more than the following: for Life Safety in	
C	NC	N/A	T	Low or Moderate Seismicity 3 times the least dimension of the chimney for Life Safety	
	110	1 1/11		in High Seismicity and for Position Retention in any calemicity 2 times the least	
				dimension of the chimpey	
<u> </u>				LID I MILLS I MIL DD I MIL ANCHODACE. Maconer akimenen and and	
	NC	NT/A	TT	TIK-LIVITI, LO-LIVITI, FK-LIVITI. AINCHORAGE: Masonry chimneys are anchored	

at each floor level, at the topmost ceiling level, and at the roof.

	Project:	Five Oaks Middle School
	Project No:	21603.10
	Completed By:	Mark Ellis
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Table 17-38 - Nonstructural Checklist

Staire	
Stairs	

STAT	'US			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	HR—not required; LS—LMH; PR—LMH. STAIR ENCLOSURES: Hollow-clay tile or unreinforced masonry walls around stair enclosures are restrained out of plane and have height-to-thickness ratios not greater than the following: for Life Safety in Low or Moderate Seismicity, 15-to-1; for Life Safety in High Seismicity and for Position Retention in any seismicity, 12-to-1.	
С	NC	N/A	U	HR—not required; LS—LMH; PR—LMH. STAIR DETAILS: The connection between the stairs and the structure does not rely on post-installed anchors in concrete or masonry, and the stair details are capable of accommodating the drift calculated using the Quick Check procedure of Section 4.4.3.1 for moment-frame structures or 0.5 in. for all other structures without including any lateral stiffness contribution from the stairs.	Needs to be verified
Conte	ents ai	nd Fur	nishii	ngs	
STAT	'US			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	HR—LMH; LS—MH; PR—MH. INDUSTRIAL STORAGE RACKS: Industrial storage racks or pallet racks more than 12 ft high meet the requirements of ANSI/RMI MH 16.1 as modified by ASCE 7, Chapter 15.	
С	NC	N/A	U	HR—not required; LS—H; PR—MH. TALL NARROW CONTENTS: Contents more than 6 ft (1.8 m) high with a height-to-depth or height-to-width ratio greater than 3-to-1 are anchored to the structure or to each other.	Contents to be inspected and braced.
С	NC	N/A	U	HR—not required; LS—H; PR—H. FALL-PRONE CONTENTS: Equipment, stored items, or other contents weighing more than 20 lb (9.1 kg) whose center of mass is more than 4 ft (1.2 m) above the adjacent floor level are braced or otherwise restrained.	Contents to be inspected and braced.
С	NC	N/A	U	HR—not required; LS—not required; PR—MH. ACCESS FLOORS: Access floors more than 9 in. (229 mm) high are braced.	
С	NC	N/A	U	HR—not required; LS—not required; PR—MH. EQUIPMENT ON ACCESS FLOORS: Equipment and other contents supported by access floor systems are anchored or braced to the structure independent of the access floor.	
С	NC	N/A	U	HR—not required; LS—not required; PR—H. SUSPENDED CONTENTS: Items suspended without lateral bracing are free to swing from or move with the structure from which they are suspended without damaging themselves or adjoining components.	Contents to be inspected and braced. (Not required at Part C)
Mech	anica	l and E	lectr	ical Equipment	•
STAT	'US			EVALUATION STATEMENT	COMMENTS
С	NC	N/A	U	HR—not required; LS—H; PR—H. FALL-PRONE EQUIPMENT: Equipment weighing more than 20 lb (9.1 kg) whose center of mass is more than 4 ft (1.2 m) above the adjacent floor level, and which is not in-line equipment, is braced.	Equipment to be inspected and braced.
С	NC	N/A	U	HR—not required; LS—H; PR—H. IN-LINE EQUIPMENT: Equipment installed in line with a duct or piping system, with an operating weight more than 75 lb (34.0 kg), is supported and laterally braced independent of the duct or piping system.	Equipment to be inspected and braced.
С	NC	N/A	U	HR—not required; LS—H; PR—MH. TALL NARROW EQUIPMENT: Equipment more than 6 ft (1.8 m) high with a height-to-depth or height-to-width ratio greater than 3- to-1 is anchored to the floor slab or adjacent structural walls.	Equipment to be inspected and braced.
С	NC	N/A	U	HR—not required; LS—not required; PR—MH. MECHANICAL DOORS: Mechanically operated doors are detailed to operate at a story drift ratio of 0.01.	
С	NC	N/A	U	HR—not required; LS—not required; PR—H. SUSPENDED EQUIPMENT: Equipment suspended without lateral bracing is free to swing from or move with the structure from which it is suspended without damaging itself or adjoining components.	Equipment to be inspected and braced. (Not required at Part C)
С	NC	N/A	U	HR—not required; LS—not required; PR—H. VIBRATION ISOLATORS: Equipment mounted on vibration isolators is equipped with horizontal restraints or snubbers and with vertical restraints to resist overturning.	Needs to be verified (Not required at Part C)
С	NC	N/A	U	HR—not required; LS—not required; PR—H. HEAVY EQUIPMENT: Floor- supported or platform-supported equipment weighing more than 400 lb (181.4 kg) is anchored to the structure.	Needs to be verified (Not required at Part C)
С	NC	N/A	U	HR—not required; LS—not required; PR—H. ELECTRICAL EQUIPMENT: Electrical equipment is laterally braced to the structure	Needs to be verified

				Project:	Five Oaks Middle School
				Project No:	21603.10
				Completed By:	Mark Ellis
H	olr	ne	S	Reviewed By:	Jennifer Eggers
Tab	le 17	7-38 -	No	nstructural Checklist	
		00	110	HR_not required: I.S_not required: PR_H_CONDUIT COUPLINGS: Conduit	Components to be inspected and install
_		4 -		greater than 2.5 in. (64 mm) trade size that is attached to panels, cabinets, or other	couplers as needed.
С	NC	N/A	U	equipment and is subject to relative seismic displacement has flexible couplings or	(Not required at Part C)
				connections.	
Piping	ç				
STAT	US		1	EVALUATION STATEMENT	COMMENTS
C	NC	NI/A	T	HR—not required; LS—not required; PR—H. FLEXIBLE COUPLINGS: Fluid and gas	Components to be inspected and install
C	INC	$1N/\Lambda$	U	piping has nextone couplings.	(Not required at Part ()
				HR—not required; LS—not required; PR—H. FLUID AND GAS PIPING: Fluid and	Piping to be inspected and braced.
С	NC	N/A	U	gas piping is anchored and braced to the structure to limit spills or leaks.	(Not required at Part C)
C	NC	NI/A	П	HR-not required; LS-not required; PR-H. C-CLAMPS: One-sided C-clamps that	Needs to be verified
C	INC	11/11	0	support piping larger than 2.5 in. (64 mm) in diameter are restrained.	(Not required at Part C)
				HR—not required; LS—not required; PR—H. PIPING CROSSING SEISMIC	Needs to be verified
С	NC	N/A	U	JOINTS: Piping that crosses seismic joints or isolation planes or is connected to	(Not required at Part C)
				seismic displacements	
Ducts	;			jousnie displacements.	
STAT	US			EVALUATION STATEMENT	COMMENTS
				HR-not required; LS-not required; PR-H. DUCT BRACING: Rectangular	Equipment to be inspected and braced.
				ductwork larger than 6 ft2 (0.56 m2) in cross-sectional area and round ducts larger than	(Not required at Part C)
С	NC	N/A	U	28 in. (711 mm) in diameter are braced. The maximum spacing of transverse bracing	
				does not exceed 30 ft (9.2 m). The maximum spacing of longitudinal bracing does not exceed $(0, f_{1}, (18.2 \text{ m}))$	
				HR—not required: I.S—not required: PR—H_DUCT SUPPORT: Ducts are not	Needs to be verified
С	NC	N/A	U	supported by piping or electrical conduit.	(Not required at Part C)
				HR—not required; LS—not required; PR—H. DUCTS CROSSING SEISMIC JOINTS:	Needs to be verified
C	NC	N/A	П	Ducts that cross seismic joints or isolation planes or are connected to independent	(Not required at Part C)
C	110	1 1/ 11	C	structures have couplings or other details to accommodate the relative seismic	
<b>F</b> 1	4			displacements.	
STAT	US			EVALUATION STATEMENT	COMMENTS
0		27/4		HR—not required; LS—H; PR—H. RETAINER GUARDS: Sheaves and drums have	Elevator is hydraulic
C	NC	N/A	U	cable retainer guards.	
С	NC	N/A	U	HR-not required; LS-H; PR-H. RETAINER PLATE: A retainer plate is present at	Elevator is hydraulic
	110	11/11	Ŭ	the top and bottom of both car and counterweight.	
C	NC	NT / A	TT	HR—not required; LS—not required; PR—H. ELEVATOR EQUIPMENT:	Needs to be verified
C	NC	$1N/\Lambda$	U	anchored	
				HR—not required; LS—not required; PR—H. SEISMIC SWITCH: Elevators capable	Elevator is hydraulic
				of operating at speeds of 150 ft/min (0.30 m/min) or faster are equipped with seismic	
С	NC	N/A	U	switches that meet the requirements of ASME A17.1 or have trigger levels set to 20% of	
				the acceleration of gravity at the base of the structure and 50% of the acceleration of	
				gravity in other locations.	NT 1 . 1 . 1
C	NC	NI/A	п	HR—not required; LS—not required; PR—H. SHAFT WALLS: Elevator shaft walls are	Needs to be verified
C	INC	18/11	0	and remoted to prevent topping into the shart during strong shaking.	
0	110	27/1		HR—not required; LS—not required; PR—H. COUNTERWEIGHT RAILS: All	Elevator is hydraulic
С	NC	N/A		counterweight rails and divider beams are sized in accordance with ASME A17.1.	
				HR-not required; LS-not required; PR-H. BRACKETS: The brackets that tie the	Elevator is hydraulic
С	NC	N/A	U	car rails and the counterweight rail to the structure are sized in accordance with ASME	
				A17.1.	Elemente a la landaradia
С	NC	N/A	U	HK—not required; LS—not required; PK—H. SPKEADEK BKACKE1: Spreader	Elevator is hydraulic
_				HR—not required; LS—not required; PR—H. GO-SLOW ELEVATORS: The building	Elevator is hydraulic
С	NC	N/A	U	has a go-slow elevator system.	



# **Strengthening Scheme**

Project No. 21603.10



Page 44







#### NON-STRUCTURAL

	N1 🗖	AT INTERIOR BRICK PILASTER WITHOUT STEEL COLUMN, PROVIDE BRACING ABOVE CEILING
	N2	<ul> <li>SUPPLEMENT (E) SUPPORT AT TOP OF (E) PLUMBING WALL PER DETAIL 5/CR21</li> </ul>
NEW HSS 4 X 4 STRUT AT MEZZANINE LEVEL	N3	PROVIDE SEISMIC BRACING AT FIRE SUPPRESSION PIPING
NEW HSS TIE BETWEEN (E) CONCRETE SHEAR WALL AND TILT-UP WALL	N4	AT DROP-IN CEILINGS, PROVIDE CLEARANCE FOR SPRINKLER HEADS, SPLAY WIRE BRACIN FIXTURES
NEW CONNECTION BETWEEN (E) RB-19 AND TILT-UP WALL AT GYM	N5	INCLUDE ALLOWANCE FOR ADDITIONAL BRACING AT INTERIOR MASONRY WALLS AND PAR
NEW CONNECTIONS BETWEEN MEZZANINE FLOOR AND GYM WALL	N6 TO N15	- BRACE TALL NARROW CONTENTS - BRACE/ANCHOR FALL-PRONE CONTENTS WEIGHING MORE THAN 20LBS WHOSE CENTER
		<ul> <li>BRACE/ANCHOR FALL-FROME EQUIPMENT WEIGHING MORE THAN 20LBS WHOSE CENTER</li> <li>BRACE/ANCHOR TALL NARROW EQUIPMENT (MORE THAN 6FT HEIGH) WITH A H:W RATIO G</li> <li>BRACE IN-LINE EQUIPMENT WITH AN OPERATING WEIGHT MORE THAN 75LB.</li> <li>PROVIDE CONDUIT COUPLINGS FOR CONDUIT GREATER THAN 2.5in. THAT IS ATTACHED TO</li> <li>PROVIDE FLEXIBLE COUPLINGS FOR FLUID AND GAS PIPING</li> </ul>

- PROVIDE GAS SHUT-OFF VALVE - BRACE FLUID AND GAS PIPING
- BRACE DUCTS LARGER THAN 6 ft/2 IN CROSS SECTIONAL AREA @30FT O.C. TRANSVERSE AND 60FT O.C. LONGITUDINALLY



M1

M2

М3

M4



IG AND COMPRESSION POSTS, AND INDEPENDENT SUPPORT FOR LIGHT

TITIONS

OF MASS IS MORE THAN 4FT ABOVE THE FLOOR R OF MASS IS MORE THAN 4FT ABOVE THE FLOOR **GREATER THAN 3:1** 

O PANELS, CABINETS OR OTHER EQPT

Project: Five Oaks MS - SRGP 2022 Application

Project No: 21603.10 Date: 03/04/2022

Sketch Title: Conceptual Retrofit

Sketch No: CR-03 Revision: 00

By: ME Page 47



# STRUCTURAL FLOOR PLANS



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Project: Five Oaks MS - SRGP 2022 Application Project No: 21603.10 Date: 03/04/2022

Sketch Title: Conceptual Retrofit

Sketch No: CR-06 Revision: 00

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By:



Page 50



Date: 03/04/2022 Project: Five Oaks MS - SRGP 2022 Applic Project No: 21603.10

Ř ပို Sketch Title:

BU 00 Revisio Sketch No: CR-07

Holmes

Page 51



KILNAR STATIONERY & PRINTING CO., POSTLAND,

and the second second



# Sketch Title: Conceptual Retrofit

GYM

MEZZANINE FLOOR PLAN -

Sketch No: CR-08\_Revision: 00 By: ME

Holmes





Project: Five Oaks MS - SRGP 2022 Appl

Page 53







Date: 03/04/2022 Project No: 21603.10

Ř ы Sketch Title:

P

BE

# PARTIAL GROUND FLOOR AND FOUNDATION PLAN

E 00:0

Sketch No: CR-10 Revisio





BE

00;0

Sketch No: CR-11\_Revision

Holmes





PARTIAL GROUND FLOOR AND FOUNDATION PLAN

E BU: Sketch No: <u>CR-13</u> Revision: <u>00</u>









Sketch No: <u>CR-16</u> Revision: 00 By: ME

Holmes

03/04/2022

Date:

Project No: 21603.10

Sketch 7



Project No: 21603.10 Date: 03/04/2022

Sketch Title: Conceptual Retro

Holmes

Sketch No: CR-17 Revision: 00

# **ROOF DETAILS**









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Š 0

8 Revisio CR-20 No: Sketch

# ROOF

S **DETAIL** 











#### **Architectural Scope Notes**

#### F1 F1-A:

- Excavate for new concrete band.
- Install concrete band per structural.
- Paint exposed concrete.
- Install sheet metal flashing over top of concrete band.

#### F1-B:

- Sawcut and remove concrete paving.
- Excavate for new concrete band.
- Install concrete band per structural.
- Paint exposed concrete.
- Install sheet metal flashing over top of concrete band.
- Patch concrete paving.

#### F1-C:

- Remove and salvage bleacher system
- Remove maple flooring along wall
- Install concrete band per structural.
- Construct metal-framed spacer with painted gypsum board finish above concrete band. Match thickness of concrete band and height of bleacher system for purpose of supporting bleacher system.
- Paint exposed concrete.
- Patch maple flooring.
- Reinstall bleacher system.

#### F1-D:

F2

F3

- Salvage and reinstall (2) recessed drinking fountains.
- Install concrete band per structural.

- Construct metal-framed partition with painted gypsum board in front of concrete band. Partition to extend to 7 feet above floor.

#### F2-A (classroom/corridor, full wall replacement):

- Salvage and reinstall miscellaneous electrical outlets, switches, data outlets, fire alarm outlets.
- Salvage and reinstall clock and chalkboard in classroom.
- Salvage plastic laminate wainscot panels and demolish aluminum trim on corridor side of wall.
- Remove 2x4 ceiling panels and grid back 3 feet each side of wall.
- Sawcut and remove concrete floor slab along length of each side of wall.
- Excavate for new footing.
- Demolish existing wall and replace with CMU wall per structural.
- Install metal furring with painted gypsum board finish each side of wall.
- Reinstall 2x4 ceiling system.
- Patch and polish concrete floor in corridor.
- Patch carpeting in classroom.
- Reinstall plastic laminate wainscot panels and install new aluminum trim on corridor side of wall.

- Salvage and reinstall doors and frames where occurring (Corridor C120J).

- Salvage and reinstall tackboards where occurring (Corridor C120J).
- Recreate mural where occurring (Corridor C120J).

#### F2-B (classroom/classroom, full wall replacement):

- Salvage and reinstall miscellaneous electrical outlets, switches, data outlets, fire alarm devices, wall speaker.
- Salvage and reinstall tackboards.
- Salvage and reinstall acoustical wall panels.
- Demolish VCT flooring along each side of wall.
- Sawcut and remove concrete floor slab along length of each side of wall.
- Excavate for new footing.
- Demolish existing wall and replace with CMU wall per structural.
- Install metal furring with painted gypsum board finish each side of wall.
- Patch VCT flooring.
- Salvage and reinstall door and frame.

#### F4 F4-A:

- Salvage and reinstall miscellaneous electrical outlets, switches, data outlets, fire alarm devices.

- Salvage and reinstall clock (Teacher Planning D101)
- Demolish existing gypsum board finish on one side of wall.
- Remove 2x4 ceiling panels and grid back 3 feet.
- Install SureBoard on wall framing per structural
- Reinstall 2x4 ceiling system.

#### F5-A: F5

- Selectively demolish existing gypsum board and framing at mechanical loft/soffit.

- Modify mechanical equipment and ductwork as necessary to install column.

- Remove maple flooring at column base.
- Sawcut and remove concrete slab for column connection to foundation.
- Install steel column per structural
- Patch and repair gypsum board and framing at mechanical loft/soffit.
- Patch concrete slab.
- Patch maple flooring.
- Paint column where exposed to view.

#### F6-A:

F6

F7

F8

- Paint bolts where exposed to view.



- Remove paint from existing steel structure where new steel plates are to be installed.

- Paint new steel plates.

#### F8-A (corridor, one side of wall):

- Salvage and reinstall miscellaneous electrical outlets, switches, data outlets, fire alarm devices.

- Remove 2x4 ceiling panels and grid back 3 feet.
- Sawcut and remove concrete floor slab along length of wall. Excavate for new footing.
- Salvage plastic laminate wainscot panels and demolish aluminum trim.
- Demolish existing gypsum board finish on one side of wall and construct
- adjacent CMU wall per structural.
- Install metal furring with painted gypsum board finish.
- Reinstall 2x4 ceiling system.
- Patch and polish concrete floor.
- Reinstall plastic laminate wainscot panels and install new aluminum trim.

#### F8-B (corridor, one side of wall):

- Demolish decorative brick pier
- Install new decorative brick pier after completion of new shear wall

#### <u>F8-C</u> (classroom, one side of wall)

- Salvage and reinstall miscellaneous electrical outlets, switches, data outlets, fire alarm devices,

- Remove 2x4 ceiling panels and grid back 3 feet.
- Sawcut and remove concrete floor slab along length of wall. Excavate for new footing.
- Demolish existing gypsum board finish on one side of wall and construct adjacent CMU wall per structural.
- Install metal furring with painted gypsum board finish.
- Reinstall 2x4 ceiling system.
- Patch carpeting.

# M1 M1-A: M2 M2-A: М3 M3-A: M4 M4-A: R1

R2 R3 R9 R10

R5-A:

R5-B:

R5-C:

R8-A:

R8-B:

R5

R6

R7

R8

- Paint steel struts.

- Demolish 2x4 ceiling system and lighting. - Install HSS tie per structural.

- Install new 2x4 ceiling system and lighting.

- Architectural scope included under R11-B.

- Demolish hard lid ceiling back from wall 2 feet. - Install weld connections per structural. - Patch and repair hard lid ceiling.

R3-A (open ceilings):

- Remove and salvage lighting, speakers, and basketball hoops.

- Install steel members at underside of gym roof per structural.

- Paint all exposed steel members.

- Reinstall lighting, speakers, and basketball hoops.

- Include allowance for selectively relocating light fixtures.

<u>R3-B</u> (dropped ceilings at mezzanine)

- Remove and salvage 2x4 ceiling panels. Disassemble ceiling grid and salvage lighting as necessary for structural work.

- Install steel members at underside of roof deck per structural.

- Reinstall 2x4 ceiling system and lighting.

- Demolish hard lid ceiling and 1x1 acoustical tiles (where occurring). Remove and salvage lighting for access to underside of roof deck. - Install steel members at underside of roof deck per structural. - Patch ceiling, install new 1x1 acoustical tiles (where occurring), and reinstall lighting.

- Remove and salvage 2x4 ceiling panels. Dissassemble ceiling grid and salvage lighting as necessary for structural work. - Install steel members at underside of roof deck per structural. - Reinstall 2x4 ceiling system and lighting.

- Install steel members at underside of roof deck per structural. - Paint steel members.

- Salvage and reinstall rooftop mechanical equipment and roof drains. - Demolish roofing to steel deck and weld deck to steel members per structural.

- Install new deck sheathing, vapor retarder, R-30 insulation, cover board, single-ply roof membrane, and flashing.

- Salvage and reinstall rooftop mechanical equipment and roof drains. - Demolish roofing to steel deck and weld deck to steel members per structural.

- Patch roof with new deck sheathing, vapor retarder, insulation (match existing R-18 thickness), cover board, and 2-ply SBS roofing.

#### Architectural Scope Notes

#### R11 <u>R11-A</u>:

- Demolish hard lid ceiling and 1x1 acoustical tiles back 3 feet for access.
- Install new connections per structural.
- Patch ceiling and install new 1x1 acoustical tiles.

#### <u>R11-B</u>:

- Remove and salvage 2x4 ceiling panels. Disassemble and salvage grid
- as necessary for access.
- Install new connections per structural.
- Reinstall 2x4 ceiling system.

#### R12 <u>R12-A</u>:

- Remove and salvage exterior soffit panels for access for structural work.
- Make new beam-column connection per structural.
- Reinstall salvaged exterior soffit panels.

#### <u>R12-B</u>:

- Architectural scope included under R11-A and R11-B.

#### R13 <u>R13-A</u>:

N1

- Remove and salvage 2x4 ceiling panels. Disassemble and salvage grid
- as necessary for access.
- Install new connections per structural.
- Reinstall 2x4 ceiling system.

#### <u>N1-A</u>:

- Remove and salvage 2x4 ceiling panels for access above ceiling.
- Install bracing at brick pilaster per structural.
- Reinstall 2x4 ceiling panels.

#### N2 <u>N2-A</u>:

- Demolish hard lid ceiling back from wall 2 feet.
- Install supplemental wall support per structural.
- Patch and repair hard lid ceiling.

#### <u>N3-A</u>:

- Remove and salvage 2x4 ceiling panels for access above ceiling. At hard lid ceilings, cut holes in ceiling for access to sprinkler piping.
- Install sprinkler system bracing per structural.
- Reinstall 2x4 ceiling panels. At hard lid ceilings, patch access holes to match existing finishes.
- At 2x4 grid ceilings, install oversized escutcheons at sprinkler head penetrations.
- N4

N3

<u>N4-A</u>: At nonstructural "position retention" zones noted on sheet CR-02 (zones A and B), provide the following:

- Remove and salvage 2x4 ceiling panels for access above ceiling.
- Install ceiling system bracing per structural.
- Modify edge details of grid system and install wide edge angle to allow movement per code.
- Reinstall 2x4 ceiling panels
- Install oversized escutcheons at sprinkler head penetrations.

Page 67



# **Itemized Construction Cost Estimate**



Project No. 21603.10

BPS SRGP 2022 - Five Oaks Middle School Conceptual March 18, 2022 Revised April 7, 2022





**Prepared for Holmes Structures** 



www.ccorpusa.com PHONE: 206-876-8008

#### TABLE OF CONTENTS

	Page
1. Project Introduction	
Executive Summary	3
Approach & Methodology	4
2. Cost Summaries	
Summary	6
Summary Matrix	7
3. Control Areas	
Controls	13
4. Construction Cost Back Up	
Building Part A	14
Building Part B	25
Building Part C	35
Building Part D	44

#### **EXECUTIVE SUMMARY**

#### 1.1 Introduction

This estimate has been prepared, pursuant to an agreement between Holmes Structures and Cumming, for the purpose of establishing a probable cost of construction at the conceptual stage.

The project scope encompasses a comprehensive seismic retrofit of structural, architectural, mechanical, plumbing, and electrical systems.

#### **1.2 Project Schedule**

	Start	Finish	Duration
Construction	Jun-23	Sep-23	4 months

#### **1.3 Market Volatility**

The ongoing novel Coronavirus (COVID-19) pandemic together with the current crisis in Ukraine are having an impact on global financial markets and the material supply chain.

Market activity is being impacted in many sectors and circumstances remain very fluid and variable in different jurisdictions. Accordingly, as of this date, we are concerned with the market related impacts on the deliverables we are furnishing to you as part of our Services including cost estimates and budgets ("Deliverable(s)"). Indeed, the current response to these issues means that we are faced with an unprecedented set of circumstances on which to base a judgement of the effects on the availability of labor, materials, and other impacts, although we are monitoring those on a continuing basis.

Given the unknown future impact that the current situations might have on the construction and real estate markets, we recommend that you keep the Deliverables of this project under frequent review. For your information, we have not added or considered additional contingency within this "Deliverable"

#### 1.4 Key Assumptions & Exclusions

This document should be read in association with *Approach & Methodology* which outline assumptions, project understanding, approach, and cost management methodology. Key assumptions built into the above cost breakdown include

#### Key Assumptions

- Design / Bid / Build
- Single Phase Construction

Key Exclusions

- Project Soft Costs
- Department Relocation
- Sttuctural Modifications to Building Part E
- Allowance for COVID-19 impacts
- Allowance for Russia/Ukraine conflict impacts
| Basis of Estimate        | - Documents used:  |
|--------------------------|--|
|                          | - Drawings   |
|                          | - Five Oaks MS - Conceptual Seismic Retrofit 3-4-2022-Struct+Arch+Parts, dated 03/04/22  |
|                          | - Other  |
|                          | - Various photos, 219 total - IMG_1823 to IMG_2042   |
| Estimate Format          | A component cost classification format has been used for the preparation of this estimate. It classifies costs by trade.   |
| Cost Mark Ups            | The following % mark ups have been included in each design option:   |
|                          | - General Conditions (10.00% on direct costs)  |
|                          | - General Requirements (4.00% compound)  |
|                          | - Bonds & Insurance (2.00% compound)   |
|                          | - Contractor's Fee (5.00% compound)  |
|                          | - Design Contingency (20.00% compound)   |
|                          | - Escalation to MOC, 08/15/23 (8.99% compound)   |
| Escalation               | All subcontract prices herein are reflective of current bid prices. Escalation has been included on the  |
|                          | summary level to the stated mid point of construction.   |
| Design Contingency       | An allowance of 20% for undeveloped design details has been <u>included</u> in this estimate. As the design of each system is further developed, details which historically increase cost become apparent  |
|                          | and must be incorporated into the estimate while decreasing the % burden.  |
| Construction Contingency | It is prudent for all program budgets to include an allowance for change orders which occur during the construction phase. These change orders normally increase the cost of the project. It is recommended that a 10% to 15% construction contingency is carried in this respect. This cost is <i>not</i> included within the estimate.   |
| Construction Schedule    | Costs included herein have been based upon a construction period of 3 months. Any costs for excessive overtime to meet accelerated schedule milestone dates are not included in this estimate.   |
| Method of Procurement    | The estimate is based on a Design/Bid/Build procurement stategy.   |
| Bid Conditions           | This estimate has been based upon competitive bid situations (minimum of 3 bidders) for all items of subcontracted work.   |
| Basis For Quantities     | Wherever possible, this estimate has been based upon the actual measurement of different items of work. For the remaining items, parametric measurements were used in conjunction with other projects of a similar nature.   |
| Basis for Unit Costs     | Unit costs as contained herein are based on current bid prices in the Beaverton / Portland, OR area.<br>Sub overheads and profit are included in each line item unit cost. Their overhead and profit covers<br>each sub's cost for labor burden, materials, and equipment, field overhead, home office overhead,<br>and profit. The general contractor's overhead is shown separately on the master summary. |

**APPROACH & METHODOLOGY** 

#### APPROACH & METHODOLOGY

Sources for Pricing	This estimate was prepared by a team of qualified cost consultants experienced in estimating construction costs at all stages of design. These consultants have used pricing data from Cumming's construction database, updated to reflect current conditions in Beaverton, OR.
Key Exclusions	The following items have been excluded from our estimate: - Project Soft Costs - Department Relocation - Allowance for COVID-19 impacts - Allowance for Russia/Ukraine conflict impacts
Items Affecting Cost Estimate	<ul> <li>Items which may change the estimated construction cost include, but are not limited to:</li> <li>Modifications to the scope of work included in this estimate.</li> <li>Unforeseen sub-surface conditions.</li> <li>Restrictive technical specifications or excessive contract conditions.</li> <li>Any specified item of material or product that cannot be obtained from 3 sources.</li> <li>Any other non-competitive bid situations.</li> <li>Bids delayed beyond the projected schedule.</li> </ul>
Statement of Probable Cost	Cumming has no control over the cost of labor and materials, the general contractor's or any subcontractor's method of determining prices, or competitive bidding and market conditions. This estimate is made on the basis of the experience, qualifications, and best judgement of a professional consultant familiar with the construction industry. Cumming, however, cannot and does not guarantee that proposals, bids, or actual construction costs will not vary from this or subsequent cost estimates. Cumming's staff of professional cost consultants has prepared this estimate in accordance with generally accepted principles and practices. This staff is available to discuss its contents with any interested party.
	Pricing reflects probable construction costs obtainable in the project locality on the target dates specified and is a determination of fair market value for the construction of this project. The estimate is not a prediction of low bid. Pricing assumes competitive bidding for every portion of the construction work for all sub and general contractors with a range of 3 - 4 bidders for all items of work. Experience and research indicates that a fewer number of bidders may result in higher bids. Conversely, an increased number of bidders may result in more competitive bid day responses.
Recommendations	Cumming recommends that the Owner and the Architect carefully review this entire document to ensure it reflects their design intent. Requests for modifications of any apparent errors or omissions to this document must be made to Cumming within ten days of receipt of this estimate. Otherwise, it will be assumed that its contents have been reviewed and accepted. If the project is over budget or there are unresolved budget issues, alternate systems / schemes should be evaluated before proceeding into further design phases.
	It is recommended that there are preparations of further cost estimates throughout design by Cumming to determine overall cost changes since the preparation of this preliminary estimate. These future estimates will have detailed breakdowns indicating materials by type, kind, and size, priced by their respective units of measure.

SUM	MARY		
Element	Area	Cost / SF	Total
Building Part A	25,324	\$122.94	\$3,113,407
Building Part B	55,783	\$41.00	\$2,287,177
Building Part C	66,068	\$46.19	\$3,051,877
Building Part D	8,100	\$0.97	\$7,877
Total Estimated Construction Cost	155,276	\$54.49	\$8,460,338
Add Alternates			Total
Alternate Schedule - Work Delayed to Summer 2024	155,276	\$2.72	\$423,017

#### BPS SRGP 2022 - Five Oaks Middle School Beaverton, Oregon Conceptual

	Building P	Building Part A		art B
Flement	Total	Cost/SF	Total	Cost/SF
		00010.	, etai	
1 F1 - Connect Tilt-up Walls to Foundations	\$197,087	\$7.78		
2 F2 - Demo + CMU Shear Wall			\$29,160	\$0.52
3 F3 - Shear Wall Footing			\$14,676	\$0.26
4 F4 - Sheath Wall				
5 F5 - 18" Steel Column	\$23,612	\$0.93		
6 F6 - Anchor Columns				
7 F7 - Strengthen Portal Frames				
8 F8 - CMU Shear Wall			\$119,751	\$2.15
9 M1 - Mezzanine HSS Strut	\$2,334	\$0.09	\$2,073	\$0.04
10 M2 - HSS Tie	\$732	\$0.03	\$2,392	\$0.04
11 M3 - Tilt-up Wall Connection	\$573	\$0.02	\$1,955	\$0.04
12 M4 - Gym Wall / Mezzanine Floor Connections	\$9,570	\$0.38		
13 R1 - Out-of-Plane Connection at Gym Roof	\$23,650	\$0.93		
14 R2 - Out-of-Plane Connection at Gym Roof Pilasters	\$43,066	\$1.70		
15 R3 - Channel Cross Bracing across Gym Roof	\$388,148	\$15.33		
16 R5 - Out-of-Plane Connection under Metal Deck			\$188,609	\$3.38
17 R6 - HSS Drag Tie			\$53,152	\$0.95
18 R7 - Angle under HSS Drag			\$1,360	\$0.02
19 R8 - R&R Roofing to Weld Metal Deck to Steel Members	\$919,542	\$36.31	\$362,555	\$6.50
20 R9 - Struts at Top of Column	\$573	\$0.02		
21 R10 - HSS Strut at Main Building	\$409	\$0.02		
22 R11 - Connect Main Building Roof and Gym Wall			\$28,513	\$0.51
23 R12 - Connect between Main Building Beam and Gym Wall			\$4,260	\$0.08
24 R13 - Allowance for New Connections			\$12,440	\$0.22
25 N1 - Bracing above Ceiling at Interior Brick Pilaster				
26 N2 - Supplement Support at top of Plumbing Wall	\$2,801	\$0.11		
27 N3 - Fire Suppression Piping Seismic Bracing	\$79,011	\$3.12	\$201,934	\$3.62
28 N4 - Drop-in Ceiling Seismic	\$54,043	\$2.13	\$167,349	\$3.00
29 N5 - Bracing at Interior Masonry Walls and Partitions	\$25,324	\$1.00	\$27,892	\$0.50
30 N6 - Brace Tall Narrow Contents	\$12,662	\$0.50	\$13,946	\$0.25
31 N7 - Brace/Anchor Fall-Prone Contents over 20 lbs	\$6,331	\$0.25	\$5,578	\$0.10
32 N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs	\$6,331	\$0.25	\$8,367	\$0.15
33 N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High	\$8,863	\$0.35	\$8,367	\$0.15
34 N10 - Brace in-Line Equipment over 75 lb	\$12,662	\$0.50	\$11,157	\$0.20
35 N11 - Conduit Couplings for Conduit over 1.5 in	\$15,000	\$0.59		
36 N12 - Flexible Couplings for Fluid and Gas Pipe	\$6,000	\$0.24		
37 N13 - Gas Shut-off Valve	\$1,200	\$0.05		
38 N14 - Brace Fluid and Gas Piping	\$22,792	\$0.90	\$11,157	\$0.20
39 N15 - Brace Ducts Larger Than 6 sf Cross-Section	\$17,220	\$0.68	\$11,157	\$0.20
40 Hazmat Abatement Allowance	\$63,310	\$2.50	\$139,458	\$2.50

		Building Pa	art A	Building Pa	art B
		25,324 SF 55,783 S		F	
Element		Total	Cost/SF	Total	Cost/SF
Subtotal Cost		\$1,942,846	\$76.72	\$1,427,257	\$25.59
General Conditions	10.0%	\$194,285	\$7.67	\$142,726	\$2.56
General Requirements	4.0%	\$85,485	\$3.38	\$62,799	\$1.13
Bonds & Insurance	2.0%	\$44,452	\$1.76	\$32,656	\$0.59
Contractor's Fee	5.0%	\$113,353	\$4.48	\$83,272	\$1.49
Design Contingency	20.0%	\$476,084	\$18.80	\$349,742	\$6.27
Escalation to MOC, 08/15/23	9.0%	\$256,901	\$10.14	\$188,725	\$3.38
Total Estimated Construction Cost		\$3,113,407	\$122.94	\$2,287,177	\$41.00

#### BPS SRGP 2022 - Five Oaks Middle School Beaverton, Oregon Conceptual

	Building Part C		Building F	Part D
	66,068 \$	SF	8,100 \$	SF
Element	Total	Cost/SF	Total	Cost/SF
1 F1 - Connect Tilt-up Walls to Foundations			\$300	\$0.04
2 F2 - Demo + CMU Shear Wall	\$104,953	\$1.59		
3 F3 - Shear Wall Footing	\$57,307	\$0.87		
4 F4 - Sheath Wall	\$12,540	\$0.19		
5 F5 - 18" Steel Column				
6 F6 - Anchor Columns			\$720	\$0.09
7 F7 - Strengthen Portal Frames			\$3,896	\$0.48
8 F8 - CMU Shear Wall	\$206,350	\$3.12		
9 M1 - Mezzanine HSS Strut				
10 M2 - HSS Tie				
11 M3 - Tilt-up Wall Connection				
12 M4 - Gym Wall / Mezzanine Floor Connections				
13 R1 - Out-of-Plane Connection at Gym Roof				
14 R2 - Out-of-Plane Connection at Gym Roof Pilasters				
15 R3 - Channel Cross Bracing across Gym Roof				
16 R5 - Out-of-Plane Connection under Metal Deck	\$320,042	\$4.84		
17 R6 - HSS Drag Tie	\$42,103	\$0.64		
18 R7 - Angle under HSS Drag	\$3,885	\$0.06		
19 R8 - R&R Roofing to Weld Metal Deck to Steel Members	\$666,253	\$10.08		
20 R9 - Struts at Top of Column				
21 R10 - HSS Strut at Main Building				
22 R11 - Connect Main Building Roof and Gym Wall				
23 R12 - Connect between Main Building Beam and Gym Wall				
24 R13 - Allowance for New Connections				
25 N1 - Bracing above Ceiling at Interior Brick Pilaster	\$4,096	\$0.06		
26 N2 - Supplement Support at top of Plumbing Wall				
27 N3 - Fire Suppression Piping Seismic Bracing	\$206.132	\$3.12		
28 N4 - Drop-in Ceiling Seismic	. ,			
29 N5 - Bracing at Interior Masonry Walls and Partitions	\$33,034	\$0.50		
30 N6 - Brace Tall Narrow Contents	\$16.517	\$0.25		
31 N7 - Brace/Anchor Fall-Prone Contents over 20 lbs	\$6.607	\$0.10		
32 N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs	\$9.910	\$0.15		
33 N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High	\$9.910	\$0.15		
34 N10 - Brace in-Line Equipment over 75 lb	\$13.214	\$0.20		
35 N11 - Conduit Couplings for Conduit over 1.5 in	· - )			
36 N12 - Flexible Couplings for Fluid and Gas Pipe				
37 N13 - Gas Shut-off Valve				
38 N14 - Brace Fluid and Gas Piping	\$13.214	\$0.20		
39 N15 - Brace Ducts Larger Than 6 sf Cross-Section	\$13.214	\$0.20		
40 Hazmat Abatement Allowance	\$165,170	\$2.50		

		Building Pa	art C	Building F	Part D
		66,068 S	F	8,100 \$	SF
Element		Total	Cost/SF	Total	Cost/SF
Subtotal Cost		\$1,904,450	\$28.83	\$4,916	\$0.61
General Conditions	10.0%	\$190,445	\$2.88	\$492	\$0.06
General Requirements	4.0%	\$83,796	\$1.27	\$216	\$0.03
Bonds & Insurance	2.0%	\$43,574	\$0.66	\$112	\$0.01
Contractor's Fee	5.0%	\$111,113	\$1.68	\$287	\$0.04
Design Contingency	20.0%	\$466,676	\$7.06	\$1,205	\$0.15
Escalation to MOC, 08/15/23	9.0%	\$251,824	\$3.81	\$650	\$0.08
Total Estimated Construction Cost		\$3,051,877	\$46.19	\$7,877	\$0.97

	Overall To	tals
Element	Total	Cost/SF
1 F1 - Connect Tilt-up Walls to Foundations	\$197.387	\$1.27
2 F2 - Demo + CMU Shear Wall	\$134,113	\$0.86
3 F3 - Shear Wall Footing	\$71,982	\$0.46
4 F4 - Sheath Wall	\$12,540	\$0.08
5 F5 - 18" Steel Column	\$23,612	\$0.15
6 F6 - Anchor Columns	\$720	\$0.00
7 F7 - Strengthen Portal Frames	\$3,896	\$0.03
8 F8 - CMU Shear Wall	\$326,102	\$2.10
9 M1 - Mezzanine HSS Strut	\$4,407	\$0.03
10 M2 - HSS Tie	\$3,124	\$0.02
11 M3 - Tilt-up Wall Connection	\$2,528	\$0.02
12 M4 - Gym Wall / Mezzanine Floor Connections	\$9,570	\$0.06
13 R1 - Out-of-Plane Connection at Gym Roof	\$23,650	\$0.15
14 R2 - Out-of-Plane Connection at Gym Roof Pilasters	\$43,066	\$0.28
15 R3 - Channel Cross Bracing across Gym Roof	\$388,148	\$2.50
16 R5 - Out-of-Plane Connection under Metal Deck	\$508,650	\$3.28
17 R6 - HSS Drag Tie	\$95,255	\$0.61
18 R7 - Angle under HSS Drag	\$5,245	\$0.03
19 R8 - R&R Roofing to Weld Metal Deck to Steel Members	\$1,948,350	\$12.55
20 R9 - Struts at Top of Column	\$573	\$0.00
21 R10 - HSS Strut at Main Building	\$409	\$0.00
22 R11 - Connect Main Building Roof and Gym Wall	\$28,513	\$0.18
23 R12 - Connect between Main Building Beam and Gym Wall	\$4,260	\$0.03
24 R13 - Allowance for New Connections	\$12,440	\$0.08
25 N1 - Bracing above Ceiling at Interior Brick Pilaster	\$4,096	\$0.03
26 N2 - Supplement Support at top of Plumbing Wall	\$2,801	\$0.02
27 N3 - Fire Suppression Piping Seismic Bracing	\$487,078	\$3.14
28 N4 - Drop-in Ceiling Seismic	\$221,392	\$1.43
29 N5 - Bracing at Interior Masonry Walls and Partitions	\$86,250	\$0.56
30 N6 - Brace Tall Narrow Contents	\$43,125	\$0.28
31 N7 - Brace/Anchor Fall-Prone Contents over 20 lbs	\$18,516	\$0.12
32 N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs	\$24,609	\$0.16
33 N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High	\$27,141	\$0.17
34 N10 - Brace in-Line Equipment over 75 lb	\$37,032	\$0.24
35 N11 - Conduit Couplings for Conduit over 1.5 in	\$15,000	\$0.10
36 N12 - Flexible Couplings for Fluid and Gas Pipe	\$6,000	\$0.04
37 N13 - Gas Shut-off Valve	\$1,200	\$0.01
38 N14 - Brace Fluid and Gas Piping	\$47,162	\$0.30
39 N15 - Brace Ducts Larger Than 6 sf Cross-Section	\$41,591	\$0.27
40 Hazmat Abatement Allowance	\$367,938	\$2.37

	Overall To	tals	
Element		Total	Cost/SF
Subtotal Cost		\$5,279,468	\$34
General Conditions	10.0%	\$527,947	\$3.40
General Requirements	4.0%	\$232,297	\$1.50
Bonds & Insurance	2.0%	\$120,794	\$0.78
Contractor's Fee	5.0%	\$308,025	\$1.98
Design Contingency	20.0%	\$1,293,706	\$8.33
Escalation to MOC, 08/15/23	9.0%	\$698,100	\$4.50
Total Estimated Construction Cost		\$8,460,338	\$54.49

#### SCHEDULE OF AREAS AND CONTROL QUANTITIES

Schedule of Areas	Building Part A B	Building Part A Building Part B Building Part C Building Part D				
1. Enclosed Areas						
Level 1	25,324	55,783	66,068	8,100	155,275	
Total Enclosed	25,324	55,783	66,068	8,100	155,275	
Total Gross Floor Area	25,324	55,783	66,068	8,100	155,275	

Building Part A

### **SUMMARY - BUILDING PART A**

Elem	ent	Tota	I	Cost / SF
01 F	-1 - Connect Tilt-up Walls to Foundations		\$197,087	\$7.78
05 F	5 - 18" Steel Column		\$23,612	\$0.93
09 N	/1 - Mezzanine HSS Strut		\$2,334	\$0.09
10 M	И2 - HSS Tie		\$732	\$0.03
11 M	//3 - Tilt-up Wall Connection		\$573	\$0.02
12 M	/4 - Gym Wall / Mezzanine Floor Connections		\$9.570	\$0.38
13 F	R1 - Out-of-Plane Connection at Gym Roof		\$23.650	\$0.93
14 F	R2 - Out-of-Plane Connection at Gym Roof Pilasters		\$43.066	\$1.70
15 F	R3 - Channel Cross Bracing across Gym Roof		\$388,148	\$15.33
19 F	R8 - R&R Roofing to Weld Metal Deck to Steel Members		\$919.542	\$36.31
20 F	R9 - Struts at Top of Column		\$573	\$0.02
21 F	R10 - HSS Strut at Main Building		\$409	\$0.02
26	V2 - Supplement Support at top of Plumbing Wall		\$2.801	\$0.11
27 1	V3 - Fire Suppression Piping Seismic Bracing		\$79.011	\$3.12
28 N	V4 - Drop-in Ceilina Seismic		\$54.043	\$2.13
29 N	V5 - Bracing at Interior Masonry Walls and Partitions		\$25.324	\$1.00
30 1	N6 - Brace Tall Narrow Contents		\$12.662	\$0.50
31 N	V7 - Brace/Anchor Fall-Prone Contents over 20 lbs		\$6.331	\$0.25
32 N	N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs		\$6.331	\$0.25
33 N	19 - Brace/Anchor Tall Narrow Equipment over 6 ft High		\$8.863	\$0.35
34 N	V10 - Brace in-Line Equipment over 75 lb		\$12.662	\$0.50
35 N	V11 - Conduit Couplings for Conduit over 1.5 in		\$15.000	\$0.59
36 1	V12 - Flexible Couplings for Fluid and Gas Pipe		\$6.000	\$0.24
37 N	V13 - Gas Shut-off Valve		\$1,200	\$0.05
38 N	V14 - Brace Fluid and Gas Piping		\$22,792	\$0.90
39 N	V15 - Brace Ducts Larger Than 6 sf Cross-Section		\$17.220	\$0.68
40 H	Hazmat Abatement Allowance		\$63,310	\$2.50
S	Subtotal		\$1,942,846	\$76.72
(	General Conditions	10.00%	\$194,285	\$7.67
5	Subtotal		\$2,137,131	\$84.39
(	General Requirements	4.00%	\$85,485	\$3.38
5	Subtotal		\$2,222,616	\$87.77
E	Bonds & Insurance	2.00%	\$44,452	\$1.76
ç	Subtotal		\$2,267,068	\$89.52
(	Contractor's Fee	5.00%	\$113,353	\$4.48
ę	Subtotal		\$2,380,421	\$94.00
[	Design Contingency	20.00%	\$476,084	\$18.80
S	Subtotal		\$2,856,506	\$112.80
E	Escalation to MOC, 08/15/23	8.99%	\$256,901	\$10.14
T0 <sup>-</sup>	TAL ESTIMATED CONSTRUCTION COST		\$3,113,407	\$122.94

Total Area:

25,324 SF

Element	Quantity	Unit	Unit Cost	Total
F1 - Connect Tilt-up Walls to Foundations				
F1_A				
At base of (E) tilt-up walls at gym provide 2 ft. high x 6 in. thick conc. band with 2 rows #4 @18" drill & epoxy into wall and #5 @ 12" oc drill & epoxy into (E) foundation E1-A				
Excavate & backfill for new concrete band. Install concrete band per structural (see below)	13	су	\$46.14	\$608
Paint exposed concrete.	163	sf	\$1,25	\$204
Install sheet metal flashing over top of concrete band 2/CR-6	89	lf	\$26.80	\$2,385
6"x24" concrete band	4	су	\$597.79	\$2,168
(2) continuous #4	137	lb	\$1.62	\$222
(4) If #4 @ 18" OC, drill & epoxy (2) into wall	183	lb	\$1.62	\$296
(4) drill and epoxy (2) into wall	119	ea	\$44.84	\$5.321
(3) If #5 @12" OC, drill & epoxy (1) into foundation	319	lb	\$1.62	\$517
(3) drill and epoxy (1) into wall	89	ea	\$44.84	\$3,991
F1-B				
At base of (E) tilt-up walls at gym provide 2 ft. high x 6 in. thick conc. band with 2 rows #4 @18" drill & epoxy into wall and #5 @ 12" oc drill & epoxy into (E) foundation E1-B				
Sawcut and remove concrete paving	900	sf	\$5.69	\$5 121
Excavate & backfill for new concrete band.	44	су	\$46.14	\$2,051
Paint exposed concrete.	550	sf	\$1,25	\$687
Install sheet metal flashing over top of concrete band.	300	lf	\$26.80	\$8,040
Patch concrete paving 2/CR-6	900	sf	\$17.73	\$15,957
6"x24" concrete band	12	CV	\$597.79	\$7,306
(2) continuous #4	462	lb	\$1.62	\$749
(4) If #4 @ 18" OC, drill & epoxy (2) into wall	616	lb	\$1.62	\$999
(4) drill and epoxy (2) into wall	400	ea	\$44.84	\$17.936
(3) If #5 @12" OC, drill & epoxy (1) into foundation	936	lb	\$1.62	\$1,516
(3) drill and epoxy (1) into wall	300	ea	\$44.84	\$13,452
F1-C 1/CR-6				
At base of (E) tilt-up walls at gym provide 2 ft. high x 6 in. thick conc. band with 2 rows #4 @18" drill & epoxy into wall and #5 @ 12" oc drill & epoxy into (E) foundation				
FI-U Demove and solverse blessber eveter	177	If	00 00	¢E 240
Remove and Salvage bleacher system	521	II of	φ30.00 ¢2.01	φ0,010 ¢1.067
Remove maple mooning along wall	551	SI	φ <b>Ζ.</b> 01	φ1,00 <i>1</i>
Construct metal-framed spacer with painted gypsum board finish above				
for purpose of supporting bloocher system	177	If	¢101 02	¢17 010
Paint exposed concrete.	443	sf	\$1.25	\$553

Element	Quantity	Unit	Unit Cost	Total
Patch maple flooring.	531	sf	\$28.08	\$14,910
Reinstall bleacher system	177	lf	\$35.00	\$6,195
1/CR-6				
6"x24" concrete band	7	су	\$597.79	\$4,311
(2) continuous #4	273	lb	\$1.62	\$442
(4) If #4 @ 18" OC, drill & epoxy (2) into wall	364	lb	\$1.62	\$589
(4) drill and epoxy (2) into wall	236	ea	\$44.84	\$10,582
(3) If #5 @12" OC, drill & epoxy (1) into foundation	552	lb	\$1.62	\$895
(3) drill and epoxy (1) into wall	177	ea	\$44.84	\$7,937
F1-D				
At base of (E) tilt-up walls at gym provide 2 ft. high x 6 in. thick conc. band with 2				
rows #4 @18" drill & epoxy into wall and #5 @ 12" oc drill & epoxy into (E) foundation				
F1-D				
Salvage and reinstall (2) recessed drinking fountains.	2	ea	\$370.26	\$741
Install concrete band per structural (see below)				
Construct metal-framed partition with painted gypsum board in front of				
concrete band. Partition to extend to 7 feet above floor 4/CR-6	15	lf	\$137.14	\$2,057
6"x24" concrete band	1	су	\$597.79	\$365
(2) continuous #4	23	lb	\$1.62	\$37
(4) If #4 @ 18" OC, drill & epoxy (2) into wall	31	lb	\$1.62	\$50
(4) drill and epoxy (2) into wall	20	ea	\$44.84	\$897
(3) If #5 @12" OC, drill & epoxy (1) into foundation	47	lb	\$1.62	\$76
(3) drill and epoxy (1) into wall	15	ea	\$44.84	\$673
F1-C 3/CR-6				
At base of (E) tilt-up walls at gym provide 2 ft. high x 6 in. thick conc. band with 2				
rows #4 @18" drill & epoxy into wall and #5 @ 12" oc drill & epoxy into (E)				
foundation				
F1-C				
Remove maple flooring along wall	411	sf	\$2.01	\$826
Install concrete band per structural (see below)				
Paint exposed concrete.	343	sf	\$1.25	\$428
Patch maple flooring.	411	sf	\$28.08	\$11.541
3/CR-06		•	,	÷,•
6"x24" concrete band	6	CV	\$597.79	\$3,337
(2) continuous #4	211	lb	\$1.62	\$342
(4) If #4 $\oplus$ 18" OC drill & epoxy (2) into wall	281	lb	\$1.62	\$456
(4) drill and epoxy (2) into wall	183	ea	\$44.84	\$8,191
(3) If $\#5 @ 12" OC drill & epoxy (1) into foundation$	427	lh	\$1.62	\$692
(3) drill and enoxy (1) into wall	137	ea	\$44 84	\$6 143
	107	u	ψττ.01	φ0,140
Total - F1 - Connect Tilt-up Walls to Foundations				\$197.087

Element	Quantity	Unit	Unit Cost	Total
F5 - 18" Steel Column				
F5				
New 18 in. steel column on inside face of wall (spans floor to roof). Connect to				
foundation and to roof. Bolt to (E) tilt-up wall at 24 in. O.C.	4,370	lb	\$4.12	\$18,003
Selectively demolish existing gypsum board and framing at mechanical				
loft/soffit	108	sf	\$12.00	\$1,296
Modify mechanical equipment and ductwork as necessary to install column	1	ls	\$750.00	\$750
Remove maple flooring at column base	9	sf	\$2.01	\$18
Sawcut and remove concrete slab for column connection to foundation	9	sf	\$5.69	\$51
Patch and repair gypsum board and framing at mechanical loft/soffit	108	sf	\$26 70	\$2 884
Patch concrete slab	9	sf	\$17.73	<del>پ</del> 2,004 \$160
Patch maple flooring	9	sf	\$28.08	\$253
Paint column where exposed to view	132	sf	\$1.50	\$198
Total - E5 - 18" Stool Column				\$23 612
				φ <b>2</b> 3,012
M1 - Mezzanine HSS Strut				
M1				
New HSS 4 x 4 strut at mezzanine level	477	lb	\$4.12	\$1.964
M1-A			• · · · -	+ ,
Paint steel struts	24	lf	\$5.00	\$120
Miscellaneous demolition and patching of adjacent finishes	25	sf	\$10.00	\$250
Total - M1 - Mezzanine HSS Strut				\$2,334
M2 - HSS Tie				
M2				
New HSS tie between (E) concrete shear wall and tilt-up wall	139	lb	\$4.12	\$573
M2-A		,	<b>\$</b> 0.00	<b>\$</b> 0.4
Demolish 2x4 ceiling system and lighting.	14	st	\$2.23	\$31
Install new 2x4 ceiling system and lighting	1/	sf	\$Q 15	\$128
		31	ψυ. τΟ	ψ120
Total - M2 - HSS Tie				\$732

Element	t	Quantity	Unit	Unit Cost	Total
M3 - Tilt	-up Wall Connection				
М3	New connection between (E) RB-19 and tilt-up wall at gym M3-A	139	lb	\$4.12	\$573
	Architectural scope included under R11-B				
Total	- M3 - Tilt-up Wall Connection				\$573
M4 - Gy	m Wall / Mezzanine Floor Connections				
M4	New connections between mezzanine floor and gym wall 1/CR-8				
	New steel brackets @ 4' OC, approximately 1'x1'-6"	259	lb	\$4.12	\$1,066
	Weld to US of beam R11-B	30 15	ea ea	\$29.98 \$24.58	\$899 \$369
	Remove and salvage 2x4 celling panels. Disassemble and salvage grid as necessary for access.	57	sf	\$1.11	\$63
	Install new connections per structural (see above) Reinstall 2x4 ceiling system	57	sf	\$5.15	\$294
M4-	A, 2/CR-8 New connection between mezzanine floor and gym wall				
	Demolish hard lid ceiling back from wall 2 feet	362	sf	\$3.34	\$1,209
	Install weld connections per structural (see below) Patch and repair hard lid ceiling 2/CR-8	362	sf	\$12.54	\$4,539
	Add fillet weld ea. Side of truss bearing plate to embed plate @4' OC	46	ea	\$24.58	\$1,131
Total	- M4 - Gym Wall / Mezzanine Floor Connections				\$9,570
R1 - Out	e-of-Plane Connection at Gym Roof				
R1					
	New out-of-plane connection at gym roof (2 3 x 3 x 1/4 angles at pilasters and 8 f max spacing) 1/CR-09	t			
	Per R1 location (2) L3x3x1/4 x 8' long angles, welded each end	1,984	lb	\$4.12	\$8,172
	(2) L3x3x1/4 x 18" long angles, welded to truss top chord (2) PL3/8" x 4"x8" tab plates welded to C-chapped	372	lb Ib	\$4.12 \$4.12	\$1,532 \$463
	(1) C8x18.75 x 24" long, with (4) 7/8" holes drilled	949	lb	\$4.12 \$4.12	\$3,909
	<ul><li>(4) 3/4" x 15" average thru-bolts, nuts, &amp; washers</li><li>(4) 7/8" holes drilled 12" avg through pilaster or tilt-up wall</li></ul>	88 88	ea ea	\$20.48 \$45.16	\$1,802 \$3,974

Element		Quantity	Unit	Unit Cost	Total
	Add fillet weld at existing truss bearing plate to embed plate	22	ea	\$24.58	\$541

Element	Quantity	Unit	Unit Cost	Total
R3_4				
Remove and salvage lighting, speakers, and basketball hoops.	352	sf	\$2.00	\$704
Paint all exposed steel members.	, 22	ea	\$20.00	\$440
Reinstall lighting, speakers, and basketball hoops.	352	sf	\$3.00	\$1,056
Include allowance for selectively relocating light fixtures	352	sf	\$3.00	\$1,056
Total - R1 - Out-of-Plane Connection at Gym Roof				\$23,650
R2 - Out-of-Plane Connection at Gym Roof Pilasters				
20				
New out-of-plane connection and continuity tie across gym roof at pilasters and 8				
L3x3x1/4	8,362	lb	\$5.15	\$43,066
Total - R2 - Out-of-Plane Connection at Gym Roof Pilasters				\$43,066
R3 - Channel Cross Bracing across Gym Roof				
R3	00,400			<b>\$440.000</b>
New C 4 x 7.25 channel cross bracing across entire gym roof	29,123	ID	\$5.15	\$149,983
R3-A				
Remove and salvage lighting, speakers, and basketball hoops.	12,544	sf	\$2.00	\$25,088
Install steel members at underside of gym roof per structural (see above)	E 40E	10	<b>*</b> = 00	
Paint all exposed steel members.	5,495	lT of	\$5.00 ¢2.00	\$27,475 ¢27,620
Reinstain lighting, speakers, and basketbain hoops.	12,544	5i ef	\$3.00 \$3.00	\$37,032 \$37,632
Ductwork modification allowance	12,044	ls	\$20.000.00	\$20,000
		-	¥ -,	÷ - )
R3-B				
Remove and salvage 2x4 ceiling panels. Disassemble ceiling grid and salvage	0.050		<b>AA AA</b>	<b>*</b> • • • • <b>-</b> •
lighting as necessary for structural work.	6,358	st	\$2.23	\$14,178
Install steel members at underside of root deck per structural (see above)	6 359	cf	¢0.15	¢59 176
Reinstan 2x4 cening system and lighting	0,330	51	φ <del>9</del> .15	φ <b>30,</b> 170
R&R grilles, registers, and diffusers; clean and paint	6,368	sf	\$1.34	\$8,533
R&R Electrical incidental allowance in ceiling R3-A	12,544	sf	\$0.50	\$6,272
R&R Electrical incidental allowance in ceiling R3-B	6,358	sf	\$0.50	\$3,179
Total - R3 - Channel Cross Bracing across Gym Roof				\$388,1 <u>48</u>

Element	Quantity	Unit	Unit Cost	Total
R8 - R&R Roofing to Weld Metal Deck to Steel Members				
00				
Ro Remove roofing and weld (E) deck to new steel members @ 12 in. o.c. 3/CR-9	25,324	sf	\$5.68	\$143,840
At 8' OC	0.750		¢4.40	¢ 40, 470
(1) L4X4X5/16 X 8 long angles, welded each end (1) DL2/8 x 12"x6" welded to trues ten short	9,752	ID Ib	\$4.1Z ¢4.12	\$40,178 ¢1,000
(1) PL3/8 X 12 X8 weided to truss top chord (2) DL2/8" x 4"x8" tob plotop welded to C obennel	407	ID Ib	⊅4.1∠ ¢4.12	¢6/1 ¢6/1
(2) PL3/0 X 4 X0 (ab plates we ded to C-channel (1) C8x18 75 x 24" long with (4) 7/8" holes drilled	2 286	ID Ib	⊅4.1∠ ¢1 12	۱ ۵۹4 ۲۱۸ ۵۵
(1) Cox 10.75 x 24 long, with (4) 7/0 holes diffied $(4)$ 3/4" x 15" average thru holts, puts & washers	2,200	03	ብ - 12 ቁት. 12	φ9,417 \$1 319
(4) 7/8" holes drilled 12" ava through nilaster or tiltun wall	212	60	\$45.16	φ <del>1</del> ,572 \$9,572
(1484) total If L3x3x1/4 angle welded across roof (R2)	8 362	lh	\$4 12	\$34 453
R8-A	0,002	10	ψη. ΤΖ	ψ04,400
Salvage and reinstall rooftop mechanical equipment and roof drains.				
R&R AC units for new roofing	25.324	sf	\$0.80	\$20.259
R&R roof drains and flashing at pipe penetrations	25.324	sf	\$0.55	\$13,928
Demolish roofing to steel deck and weld deck to steel members per structural (see above)	,			<i> </i>
Install new deck sheathing, vapor retarder, R-30 insulation, cover board,	,			
single-ply roof membrane, and flashing	25,324	sf	\$19.32	\$489,260
R&R Electrical on roof R8-A and B	18,966	sf	\$8.00	\$151,728
Total - R8 - R&R Roofing to Weld Metal Deck to Steel Members				\$919,542
R9 - Struts at Top of Column				
R9 Provide struts at top of new 18 in. steel column to tie in to roof framing	139	lb	\$4.12	\$573
Total - R9 - Struts at Top of Column				\$573
R10 - HSS Strut at Main Building				
R10				
New HSS strut at main building roof level. Connect ea end	99	lb	\$4.12	\$409
Total - R10 - HSS Strut at Main Building				\$409

Element	Quantity	Unit	Unit Cost	Total
N2 - Supplement Support at top of Plumbing Wall				
N2 Supplement (E) support at top of (E) plumbing wall per detail 5/CR-21 5/CR-21				
L3x3x1/4 x 8' long (assumed) @ 8' OC, welded each end N2-A	316	lb	\$3.34	\$1,054
Demolish hard lid ceiling back from wall 2 feet	110	sf	\$3.34	\$367
Patch and repair hard lid ceiling	110	sf	\$12.54	\$1,379
Total - N2 - Supplement Support at top of Plumbing Wall				\$2,801
N3 - Fire Suppression Piping Seismic Bracing				
N3-A				
Remove and salvage 2x4 ceiling panels for access above ceiling. At hard lid				
ceilings, cut holes in ceiling for access to sprinkler piping	25,324	sf	\$0.15	\$3,799
Install sprinkler system bracing per structural	25,324	sf	\$1.37	\$34,694
Reinstall 2x4 ceiling panels. At hard lid ceilings, patch access holes to match			<b>AA AA</b>	<b>•</b> · • ·
existing finishes	25,324	sf	\$0.62	\$15,701
At 2x4 grid ceilings, install oversized escutcheons at sprinkler head penetrations	25,324	st	\$0.98	\$24,818
Total - N3 - Fire Suppression Piping Seismic Bracing				\$79,011
N4 - Drop-in Ceiling Seismic				
N4-A: At nonstructural "position retention" zones noted on sheet CR-02 (zones A and B), provide the following				
Remove and salvage 2x4 ceiling panels for access above ceiling.	6,358	sf	\$0.15	\$954
Install ceiling system bracing per structural.	6,358	sf	\$0.50	\$3,179
Modify edge details of grid system and install wide edge angle to allow movement	t			
per code.	6,358	sf	\$0.25	\$1,590
Reinstall 2x4 ceiling panels	6,358	sf	\$0.62	\$3,942
Install oversized escutcheons at sprinkler head penetrations	6,358	sf	\$0.98	\$6,231
R&R Elect in ceilings covers work n3 n4	6,358	sf	\$6.00	\$38,148
Total - N4 - Drop-in Ceiling Seismic				\$54,043

Element	Quantity	Unit	Unit Cost	Total
N5 - Bracing at Interior Masonry Walls and Partitions				
Bracing at interior masonry walls and partitions - allowance	25,324	sf	\$1.00	\$25,324
Total - N5 - Bracing at Interior Masonry Walls and Partitions				\$25,324
N6 - Brace Tall Narrow Contents				
Brace tall narrow contents - allowance	25,324	sf	\$0.50	\$12,662
Total - N6 - Brace Tall Narrow Contents				\$12,662
N7 - Brace/Anchor Fall-Prone Contents over 20 lbs				
Brace/anchor fall-prone contents over 20 lbs - allowance	25,324	sf	\$0.25	\$6,331
Total - N7 - Brace/Anchor Fall-Prone Contents over 20 lbs				\$6,331
N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs				
Brace/anchor fall-prone equipment over 20 lbs - allowance	25,324	sf	\$0.25	\$6,331
Total - N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs				\$6,331
N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High				
Brace/anchor tall narrow equipment over 6 ft high - allowance	25,324	sf	\$0.35	\$8,863
Total - N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High				\$8,863
N10 - Brace in-Line Equipment over 75 lb				
Brace in-line equipment over 75 lb - allowance	25,324	sf	\$0.50	\$12,662
Total - N10 - Brace in-Line Equipment over 75 lb	·			\$12,6 <u>62</u>

#### **DETAIL ELEMENTS - BUILDING PART A** Element Quantity Unit Unit Cost Total N11 - Conduit Couplings for Conduit over 1.5 in Electrical allowance expansion joints 1 ls \$15,000.00 \$15,000 Total - N11 - Conduit Couplings for Conduit over 1.5 in \$15,000 N12 - Flexible Couplings for Fluid and Gas Pipe Flex connections 1 \$6,000.00 \$6,000 ls Total - N12 - Flexible Couplings for Fluid and Gas Pipe \$6,000 N13 - Gas Shut-off Valve Shut off valve 1 ea \$1,200.00 \$1,200 Total - N13 - Gas Shut-off Valve \$1,200 N14 - Brace Fluid and Gas Piping Pipe bracing 25.324 sf \$0.90 \$22.792 Total - N14 - Brace Fluid and Gas Piping \$22,792 N15 - Brace Ducts Larger Than 6 sf Cross-Section Duct bracing 25,324 sf \$0.68 \$17,220 Total - N15 - Brace Ducts Larger Than 6 sf Cross-Section \$17,220 Hazmat Abatement Allowance Hazmat abatement allowance 25,324 sf \$2.50 \$63,310 **Total - Hazmat Abatement Allowance** \$63,310

Building Part B

### **SUMMARY - BUILDING PART B**

Elem	ent	Tota	Cost / SF	
02	F2 - Demo + CMU Shear Wall		\$29,160	\$0.52
03	F3 - Shear Wall Footing		\$14,676	\$0.26
08	F8 - CMU Shear Wall		\$119,751	\$2.15
09	M1 - Mezzanine HSS Strut		\$2,073	\$0.04
10	M2 - HSS Tie		\$2,392	\$0.04
11	M3 - Tilt-up Wall Connection		\$1,955	\$0.04
16	R5 - Out-of-Plane Connection under Metal Deck		\$188,609	\$3.38
17	R6 - HSS Drag Tie		\$53,152	\$0.95
18	R7 - Angle under HSS Drag		\$1,360	\$0.02
19	R8 - R&R Roofing to Weld Metal Deck to Steel Members		\$362,555	\$6.50
22	R11 - Connect Main Building Roof and Gym Wall		\$28,513	\$0.51
23	R12 - Connect between Main Building Beam and Gym Wall		\$4,260	\$0.08
24	R13 - Allowance for New Connections		\$12,440	\$0.22
27	N3 - Fire Suppression Piping Seismic Bracing		\$201,934	\$3.62
28	N4 - Drop-in Ceiling Seismic		\$167,349	\$3.00
29	N5 - Bracing at Interior Masonry Walls and Partitions		\$27,892	\$0.50
30	N6 - Brace Tall Narrow Contents		\$13,946	\$0.25
31	N7 - Brace/Anchor Fall-Prone Contents over 20 lbs		\$5,578	\$0.10
32	N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs		\$8,367	\$0.15
33	N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High		\$8,367	\$0.15
34	N10 - Brace in-Line Equipment over 75 lb		\$11,157	\$0.20
38	N14 - Brace Fluid and Gas Piping		\$11,157	\$0.20
39	N15 - Brace Ducts Larger Than 6 sf Cross-Section		\$11,157	\$0.20
40	Hazmat Abatement Allowance		\$139,458	\$2.50
	Subtotal		\$1,427,257	\$25.59
	General Conditions	10.00%	\$142,726	\$2.56
	Subtotal		\$1,569,983	\$28.14
	General Requirements	4.00%	\$62,799	\$1.13
	Subtotal		\$1,632,782	\$29.27
	Bonds & Insurance	2.00%	\$32,656	\$0.59
	Subtotal		\$1,665,438	\$29.86
	Contractor's Fee	5.00%	\$83,272	\$1.49
	Subtotal		\$1,748,710	\$31.35
	Design Contingency	20.00%	\$349,742	\$6.27
	Subtotal		\$2,098,452	\$37.62
	Escalation to MOC, 08/15/23	8.99%	\$188,725	\$3.38
TO	TAL ESTIMATED CONSTRUCTION COST		\$2,287,177	\$41.00

Total Area:

55,783 SF

Elemen	t	Quantity	Unit	Unit Cost	Total
F2 - Der	no + CMU Shear Wall				
F2	<ul> <li>17' high</li> <li>Demo (E) wall and replace with (N) CMU shear wall (8 in. CMU typ uno.)</li> <li>Demolish existing wall and replace with CMU wall per structural.</li> <li>At (E) steel column, weld horiz bars to tie to new CMU wall, typ. 17' high</li> <li>F2-B</li> <li>Salvage and reinstall miscellaneous electrical outlets, switches, data outlets, fire alarm devices, wall speaker.</li> <li>Salvage and reinstall tackboards.</li> <li>Salvage and reinstall acoustical wall panels.</li> <li>Demolish VCT flooring along each side of wall.</li> <li>Excavate for new footing.</li> <li>Install metal furring with painted gypsum board finish each side of wall.</li> <li>Patch VCT flooring.</li> <li>Salvage and reinstall door and frame</li> </ul>	357 417 21 357 63 63 9 357 63 1	sf lb sf sf sf sf cy sf sf ea	\$53.44 \$4.12 \$75.00 \$0.25 \$1.00 \$0.83 \$5.69 \$46.14 \$13.15 \$5.33 \$470.51	\$19,078 \$1,718 \$1,575 \$89 \$357 \$52 \$358 \$431 \$4,695 \$336 \$471
Total	- F2 - Demo + CMU Shear Wall				\$29,160
F3 - She	ear Wall Footing				
F3	Provide (N) concrete strip footing to support (N) CMU shear wall. assume min 18in thickness and 36in width uno. provide 250 lb/cy reinforcing. demo and rebuild (E) slab as required for installation of wall and reconstruct after installation of wall. <i>In addition to F2 scope, above:</i> Reinforcing Form and place concrete footing Backfill footing Infill concrete floor slab	2,979 12 14 260	lb cy cy sf	\$1.62 \$420.03 \$17.02 \$17.73	\$4,826 \$5,005 \$234 \$4,610
Total	- F3 - Shear Wall Footing				\$14,676
F8 - CM	U Shear Wall				
F8,	8" wall, 27' high Provide (N) CMU shear wall (8 in. CMU typ uno.) adjacent to (E) wall At (E) steel column, weld horiz bars to tie to new CMU wall, typ.	945 695	sf Ib	\$34.25 \$4.12	\$32,366 \$2,864

Element	Quantity	Unit	Unit Cost	Total
F8-A				
Salvage and reinstall miscellaneous electrical outlets, switches, data outlets,				
fire alarm devices.	35	lf	\$50.00	\$1,750
Remove 2x4 ceiling panels and grid back 3 feet.	140	sf	\$1.11	\$155
Sawcut and remove concrete floor slab along length of wall. Excavate for				
new footing.				
Sawcut and remove concrete floor slab along length of wall	140	sf	\$5.69	\$797
Excavate for new footing	16	су	\$29.12	\$453
Form and place concrete footing	6	су	\$420.03	\$2,695
Backfill footing	7	су	\$17.02	\$126
Salvage plastic laminate wainscot panels and demolish aluminum trim. Demolish existing gypsum board finish on one side of wall (see structural	140	sf	\$5.00	\$700
scope above for construction of new CMU wall ).	945	sf	\$0.60	\$567
Install metal furring with painted gypsum board finish.	945	sf	\$13.15	\$12,427
Reinstall 2x4 ceiling system	140	sf	\$5.15	\$721
Patch and polish concrete floor	140	sf	\$22.44	\$3,142
Reinstall plastic laminate wainscot panels and install new aluminum trim	140	sf	\$5.00	\$700
F8, 12" wall, 27' high				
Provide (N) CMU shear wall (12 in. CMU) adjacent to (E) wall	891	sf	\$40.28	\$35,889
At (E) steel column, weld horiz bars to tie to new CMU wall, typ. F8-A	655	lb	\$4.12	\$2,700
Salvage and reinstall miscellaneous electrical outlets, switches, data outlets,	33	lf	\$50.00	\$1,650
Remove 2x4 ceiling panels and grid back 3 feet.	132	sf	\$1.11	\$147
Sawcut and remove concrete floor slab along length of wall. Excavate for	-	-	,	,
Sawcut and remove concrete floor slab along length of wall	132	sf	\$5.69	\$751
Excavate for new footing	15	су	\$29.12	\$427
Form and place concrete footing	6	cý	\$420.03	\$2,541
Backfill footing	6	cy	\$17.02	\$105
Salvage plastic laminate wainscot panels and demolish aluminum trim. Demolish existing gypsum board finish on one side of wall (see structural	132	sf	\$0.35	\$46
scope above for construction of new CMU wall ).	891	sf	\$0.60	\$535
Install metal furring with painted gypsum board finish.	891	sf	\$13.15	\$11,717
Reinstall 2x4 ceiling system.	132	sf	\$5.15	\$680
Patch and polish concrete floor.	132	sf	\$22.44	\$2,962
Reinstall plastic laminate wainscot panels and install new aluminum trim	132	sf	\$1.05	\$139
Total - F8 - CMU Shear Wall				\$119.751
				<i>•••••</i> ,•••
M1 - Mezzanine HSS Strut				
M1				
New HSS 4 x 4 strut at mezzanine level M1-A	417	lb	\$4.12	\$1,718
Paint steel struts	21	lf	\$5.00	\$105
Miscellaneous demolition and patching of adjacent finishes	25	sf	\$10.00	\$250
			÷	+200
Total - M1 - Mezzanine HSS Strut				\$2,073

Element	Quantity	Unit	Unit Cost	Total
M2 - HSS Tie				
M2				
New HSS tie between (E) concrete shear wall and tilt-up wall	437	lb	\$4.12	\$1,800
M2-A				
Demolish 2x4 ceiling system and lighting.	52	sf	\$2.23	\$116
Install HSS tie per structural (see above)	52	sf	\$9.15	\$476
install new 2x4 county system and lighting	02	01	φ0.10	ψησ
Total - M2 - HSS Tie				\$2,392
M3 - Tilt-up Wall Connection				
M3 A				
Structural allowance components	1	ls	\$1.000.00	\$1.000
Architectural scope included under R11-B		-	, ,	, ,
R11-B				
Remove and salvage 2x4 ceiling panels. Disassemble and salvage grid	as 40	of	¢1 11	¢⊑つ
Install new connections per structural	40 159	Si Ih	φ1.11 \$4.12	ათა \$655
Reinstall 2x4 ceiling system	48	sf	\$5.15	\$247
Total - M3 - Tilt-up Wall Connection				\$1,955
R5 - Out-of-Plane Connection under Metal Deck				
DE				
New out-of-plane connection and continuity ties (3 x 3 x 1/4 angle at 8 ft max	x			
spacing) At underside of metal deck.	6,001	lb	\$4.12	\$24,725
1/CR-19				
(1) at each R5 location	4 000		<b>A</b> 4.40	<b>*</b> 0.070
(1) L3x3x1/4 x 8' long angles, welded each end (1) DL2/9 x 49"x6" welded to true ton chord	1,668	lb Ib	\$4.12 \$4.12	\$6,872
(1) PL3/8 X 12 X8 weided to truss top chord (1) PL1/2 x 12"x6"	320	ID Ib	\$4.1∠ ¢4.12	\$1,34Z \$1,700
(1) FL 1/2 X 12 XU (1) FL 3/8 x 6"x6" knife plate w/ (2) 7/8" drilled holes, welded to 12x6 pla	404 163	lb lb	φ4.12 \$1.12	φ1,790 \$671
(2) 3/4" epoxy anchors	74	ea	\$29.98	\$2,219
R5-A				
Demolish hard lid ceiling and 1x1 acoustical tiles (where occurring). Remove	e and			
salvage lighting for access to underside of roof deck.	458	sf	\$4.45	\$2,038
Install steel members at underside of roof deck per structural (see above)				
Patch ceiling, install new 1x1 acoustical tiles (where occurring), and reinstall		-	•	<b>A</b>
lighting.	458	sf	\$22.10	\$10,122

Element		Quantity	Unit	Unit Cost	Total
R5-	В				
	Remove and salvage 2x4 ceiling panels. Disassemble ceiling grid and salvage lighting as necessary for structural work.	7,394	sf	\$2.23	\$16,489
	Reinstall 2x4 ceiling system and lighting	7,394	sf	\$9.15	\$67,655
R5-	c				
	Install steel members at underside of roof deck per structural (see above) Paint steel members	2,713	sf	\$2.50	\$6,783
Rer	nove and replace grilles, registers, and diffusers outlets with new including flex duct	458	sf	\$1.85	\$847
R&I	R grilles, registers, and diffusers outlets	7,062	sf	\$0.95	\$6,709
R&	R Electrical allowance in ceiling R5-A	458	sf	\$11.00	\$5,038
R&I	R Electrical allowance in ceiling R5-B	7,062	sf	\$5.00	\$35,310
Total	· R5 - Out-of-Plane Connection under Metal Deck				\$188,609
R6 - HS	S Drag Tie				
DG					
ΝU	New HSS 3 1/2 x 2 1/2 x 3/8 (assumed) drag tie at underside of metal deck. 2/CR-21	4,199	lb	\$4.12	\$17,298
	Continuous 8"Wx8"H concrete cap on new CMU wall	5	су	\$597.79	\$3,247
	(2) 3/4" dia stud embeds welded to US of new R6 HSS drag beam @ 2' OC	300	ea	\$3.87	\$1,161
	L4x4x5/16 x 8' diagonal bracing welded each end @ 8' OC	6,992	lb	\$4.12	\$28,807
R6	- 2/CR-15				
	New HSS 3 1/2 x 2 1/2 x 3/8 (assumed) drag tie at underside of metal deck.	364	lb	\$4.12	\$1,499
	PL1/2 x 3"x6" (assumed) steel tabs, w/ 7/8" holes welded to HSS 2' OC	38	lb	\$4.12	\$157
	3/4" epoxy anchors to concrete walls, 2' OC	13	ea	\$29.98	\$390
	M2-A Demolish 2x4 ceiling system and lighting.	52	sf	\$2.23	\$116
	Install HSS tie per structural (see above)		•	<b>+-</b>	<b>,,</b>
	Install new 2x4 ceiling system and lighting	52	sf	\$9.15	\$476
Total	- R6 - HSS Drag Tie				\$53,152

Element	Quantity	Unit	Unit Cost	Total
R7 - Angle under HSS Drag				
R7 New 2 1/2 x 2 1/2 x 1/4 steel angle at underside of HSS drag to support drag (at 8 ft max spacing). Weld angles to underside of top chord of (E) truss joist 3/CR-21				
(10) If L2 1/2x2 1/2x/14, welded to HSS and to US of truss top chord each end	330	lb	\$4.12	\$1,360
Total - R7 - Angle under HSS Drag				\$1,360
R8 - R&R Roofing to Weld Metal Deck to Steel Members				
R8 Remove roofing and weld (E) deck to new steel members @ 12 in. o.c.	10,233	sf	\$5.68	\$58,123
R8-B Salvage and reinstall rooftop mechanical equipment and roof drains. R&R AC units for new roofing R&R roof drains and flashing at pipe penetrations Patch roof with new deck sheathing, vapor retarder, insulation (match existing R- 18 thickness), cover board, and 2-ply SBS roofing	10,233 10,233 10,233	sf sf	\$0.80 \$0.55 \$22.40	\$8,186 \$5,628 \$229,219
R&R Electrical on roof	10,233	sf	\$6.00	\$61,398
Total - R8 - R&R Roofing to Weld Metal Deck to Steel Members				\$362,555
R11 - Connect Main Building Roof and Gym Wall				
R11 New connections between main building roof and gym wall 1/CR-20				
New steel brackets @ 4' OC, approximately 1'x1'-6" Epoxy bolt to tilt-up wall Weld to US of beam	828 96 48	lb ea ea	\$4.12 \$29.98 \$24.58	\$3,411 \$2,878 \$1,180
R11-A Demolish hard lid ceiling and 1x1 acoustical tiles back 3 feet for access. Install new connections per structural (see above) Patch ceiling and install new 1x1 acoustical tiles	204	sf	\$3.34 \$17.07	\$681 \$3.482
R11-B Remove and salvage 2x4 ceiling panels. Disassemble and salvage grid as	204	31	ψ11.UI	ψ0,402
necessary for access. Install new connections per structural (see above) Reinstall 2x4 ceiling system	296 296	sf sf	\$2.23 \$4.12	\$660 \$1,220
				· · ·

Page 100 Page 32 of 47

Element	Quantity	Unit	Unit Cost	Total
Electrical allowance expansion joints	1	ls	\$15,000.00	\$15,000
Total - R11 - Connect Main Building Roof and Gym Wall				\$28,513
R12 - Connect between Main Building Beam and Gym Wall				
R12 New connection between new HSS drag beam at main building high roof and gym wall	n 556	lb	\$4.12	\$2,291
R12-A Remove and salvage exterior soffit panels for access for structural work. Make new beam-column connection per structural (see above)	64	sf	\$7.50	\$480
Reinstall salvaged exterior somt panels	04	SI	φ23.21	<b>ֆ</b> 1,469
Total - R12 - Connect between Main Building Beam and Gym Wall				\$4,260
R13 - Allowance for New Connections				
R13 Include allowance for new connections	2,913	lb	\$4.12	\$12,000
Remove and salvage 2x4 ceiling panels. Disassemble and salvage grid as necessary for access.	572	sf	\$0.15	\$86
Reinstall 2x4 ceiling system	572	sf	\$0.62	\$355
Total - R13 - Allowance for New Connections				\$12,440
N3 - Fire Suppression Piping Seismic Bracing				
N3-A Remove and salvage 2x4 ceiling panels for access above ceiling. At hard lid			<b>A0</b> 45	<b>*</b> • • • <b>- -</b>
ceilings, cut holes in ceiling for access to sprinkler piping Install sprinkler system bracing per structural Reinstall 2x4 ceiling panels. At hard lid ceilings, patch access holes to match	55,783 55,783	st sf	\$0.15 \$1.37	\$8,367 \$76,423
existing finishes At 2x4 grid ceilings, install oversized escutcheons at sprinkler head penetrations	55,783 55,783	sf sf	\$0.62 \$0.98	\$34,585 \$54,667
R&R Elect in ceilings	55,783	sf	\$0.50	\$27,892
Total - N3 - Fire Suppression Piping Seismic Bracing				\$201,934

Element	Quantity	Unit	Unit Cost	Total
N4 - Drop-in Ceiling Seismic				
N4-A: At nonstructural "position retention" zones noted on sheet CR-02 (zones A and				
B), provide the following				
Remove and salvage 2x4 ceiling panels for access above ceiling.	55,783	sf	\$0.15	\$8,367
Install ceiling system bracing per structural.	55,783	sf	\$0.50	\$27,892
Modify edge details of grid system and install wide edge angle to allow movement				
per code.	55,783	sf	\$0.25	\$13,946
Reinstall 2x4 ceiling panels	55,783	sf	\$0.62	\$34,585
Install oversized escutcheons at sprinkler head penetrations	55,783	sf	\$0.98	\$54,667
R&R Elect in ceilings	55,783	sf	\$0.50	\$27,892
Total - N4 - Drop-in Ceiling Seismic				\$167,349
N5 - Bracing at Interior Masonry Walls and Partitions				
Bracing at interior masonry walls and partitions - allowance	55,783	sf	\$0.50	\$27,892
Total - N5 - Bracing at Interior Masonry Walls and Partitions				\$27,892
N6 - Brace Tall Narrow Contents				
Brace tall parrow contents allowance	55 783	ef	<b>¢</b> በ 25	\$13.046
	55,705	51	ψ0.25	φ10,940
Total - N6 - Brace Tall Narrow Contents				\$13,946
N7 - Brace/Anchor Fall-Prone Contents over 20 lbs				
Brace/anchor fall-prone contents over 20 lbs - allowance	55,783	sf	\$0.10	\$5,578
Total - N7 - Brace/Anchor Fall-Prone Contents over 20 lbs				\$5,578
N9 Proce/Ancher Fall Proce Fauinment ever 20 the				
No - Drace/Anchor Fail-Prone Equipment over 20 IDS				
Brace/anchor fall-prone equipment over 20 lbs - allowance	55,783	sf	\$0.15	\$8,367
Total - N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs				\$8, <u>3</u> 67

Element	Quantity	Unit	Unit Cost	Total
N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High				
Brace/anchor tall narrow equipment over 6 ft high - allowance	55,783	sf	\$0.15	\$8,367
Total - N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High				\$8,367
N10 - Brace in-Line Equipment over 75 lb				
Brace in-line equipment over 75 lb - allowance	55,783	sf	\$0.20	\$11,157
Total - N10 - Brace in-Line Equipment over 75 lb				\$11,157
N14 - Brace Fluid and Gas Piping				
Pipe bracing	55,783	sf	\$0.20	\$11,157
Total - N14 - Brace Fluid and Gas Piping				\$11,157
N15 - Brace Ducts Larger Than 6 sf Cross-Section				
Duct bracing	55,783	sf	\$0.20	\$11,157
Total - N15 - Brace Ducts Larger Than 6 sf Cross-Section				\$11,157
Hazmat Abatement Allowance				
Hazmat abatement allowance	55,783	sf	\$2.50	\$139,458
Total - Hazmat Abatement Allowance				\$139,458

Project # 22-00165.02 03/18/22

Building Part C

### **SUMMARY - BUILDING PART C**

Elem	ent	Tota	I	Cost / SF
02	F2 - Demo + CMU Shear Wall		\$104,953	\$1.59
03	F3 - Shear Wall Footing		\$57,307	\$0.87
04	F4 - Sheath Wall		\$12,540	\$0.19
08	F8 - CMU Shear Wall		\$206,350	\$3.12
16	R5 - Out-of-Plane Connection under Metal Deck		\$320,042	\$4.84
17	R6 - HSS Drag Tie		\$42,103	\$0.64
18	R7 - Angle under HSS Drag		\$3,885	\$0.06
19	R8 - R&R Roofing to Weld Metal Deck to Steel Members		\$666,253	\$10.08
25	N1 - Bracing above Ceiling at Interior Brick Pilaster		\$4,096	\$0.06
27	N3 - Fire Suppression Piping Seismic Bracing		\$206,132	\$3.12
29	N5 - Bracing at Interior Masonry Walls and Partitions		\$33,034	\$0.50
30	N6 - Brace Tall Narrow Contents		\$16,517	\$0.25
31	N7 - Brace/Anchor Fall-Prone Contents over 20 lbs		\$6,607	\$0.10
32	N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs		\$9,910	\$0.15
33	N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High		\$9,910	\$0.15
34	N10 - Brace in-Line Equipment over 75 lb		\$13,214	\$0.20
38	N14 - Brace Fluid and Gas Piping		\$13,214	\$0.20
39	N15 - Brace Ducts Larger Than 6 sf Cross-Section		\$13,214	\$0.20
40	Hazmat Abatement Allowance		\$165,170	\$2.50
	Subtotal		\$1,904,450	\$28.83
	General Conditions	10.00%	\$190,445	\$2.88
	Subtotal		\$2,094,895	\$31.71
	General Requirements	4.00%	\$83,796	\$1.27
	Subtotal		\$2,178,691	\$32.98
	Bonds & Insurance	2.00%	\$43,574	\$0.66
	Subtotal		\$2,222,264	\$33.64
	Contractor's Fee	5.00%	\$111,113	\$1.68
	Subtotal		\$2,333,378	\$35.32
	Design Contingency	20.00%	\$466,676	\$7.06
	Subtotal		\$2,800,053	\$42.38
	Escalation to MOC, 08/15/23	8.99%	\$251,824	\$3.81

#### TOTAL ESTIMATED CONSTRUCTION COST

Total Area:

66,068 SF

\$3,051,877

\$46.19

Element	Quantity	Unit	Unit Cost	Total
F2 - Demo + CMU Shear Wall				
F2 - 1/CR-15				
1/CR-15				
At 8' OC				
Continuous 8"Wx12"H concrete cap on new CMU wall	2	су	\$597.79	\$934
(2) 3/4" dia stud embeds welded to US of (E) steel beam	14	ea	\$3.87	\$54
L4x4x5/16 x 8' diagonal bracing welded each end	1,288	lb	\$4.12	\$5,307
F2, 17' high				
Demo (E) wall and replace with (N) CMU shear wall (8 in. CMU typ uno.)				
Demolish existing wall and replace with CMU wall per structural.	935	sf	\$53.44	\$49,966
At (E) steel column, weld horiz bars to tie to new CMU wall, typ. 17' high F2-A	1,092	lb	\$4.12	\$4,500
Salvage and reinstall miscellaneous electrical outlets, switches, data outlets,				
fire alarm outlets.	55	sf	\$75.00	\$4,125
Salvage and reinstall clock and chalkboard in classroom.	1	ls	\$150.00	\$150
Salvage plastic laminate wainscot panels and demolish aluminum trim on				
corridor side of wall.	220	sf	\$5.00	\$1,100
Remove 2x4 ceiling panels and grid back 3 feet each side of wall.	440	sf	\$1.11	\$488
Install metal furring with painted gypsum board finish each side of wall.	1,870	sf	\$13.15	\$24,591
Reinstall 2x4 ceiling system.	330	sf	\$5.15	\$1,700
Patch and polish concrete floor in corridor.	165	sf	\$22.44	\$3,703
Patch carpeting in classroom.	165	sf	\$5.55	\$916
Reinstall plastic laminate wainscot panels and install new aluminum trim on				
corridor side of wall.	220	sf	\$5.00	\$1,100
Salvage and reinstall doors and frames where occurring (Corridor C120J).	3	ea	\$470.51	\$1,412
Salvage and reinstall tackboards where occurring (Corridor C120J).	935	sf	\$0.25	\$234
Recreate mural where occurring (Corridor C120J).	935	sf	\$5.00	\$4,675
Total - F2 - Demo + CMU Shear Wall				\$104,953
E3 - Shear Wall Footing				
F3				
19 this this concrete strip tooling to support (N) CMO shear wall, assume min				
roll thickness and soll with the provide 250 b/cy remoting, denoted and required ( $\Gamma$ ) also as required for installation of well and reconstruct after installation				
UI wall.	050	<u>م</u>	¢5 60	¢1 010
Sawcul and remove concrete moor stab	002	SI	\$0.09 \$46.44	Φ4,040 ¢4,200
Excavate for new looting.	95	CY	ቅ40.14 ድኅ ድን	¢4,300 ¢15 015
Remotony	3,103	u ov	∠۵.1 ¢ د ۱.۵۵	010,015 ¢16 100
Form and place concrete rooting	39	Cy	Φ42U.U3 ¢47.00	φ10,4UZ ¢700
Daukiili luuliily Infill concrete floor clab	45	cy	φ11.UZ ¢17.72	۵۵/۴ ۵۵/۴ ۲۵
	002	SI	\$11.13	φ15,100

Total - F3 - Shear Wall Footing	\$57,307

Element	Quantity	Unit	Unit Cost	Total
F4 - Sheath Wall				
F1				
Provide new sureboard sheathing (one side only) from ground floor to underside of fan room floor. provide additional connections from (E) metal stud framing to slab below, floor above and steel posts at ends of walls F4-A				
Salvage and reinstall miscellaneous electrical outlets, switches, data outlets,	4 405		<b>*</b> = 00	
fire alarm devices.	1,105	st	\$5.00 \$50.00	\$5,525 ¢50
Demolish existing gynsum board finish on one side of wall	1 105	ea sf	\$0.00 \$0.60	\$663
Remove 2x4 ceiling panels and grid back 3 feet.	260	sf	\$1.11	\$289
Install SureBoard on wall framing per structural	1,105	sf	\$4.23	\$4,674
Reinstall 2x4 ceiling system	260	sf	\$5.15	\$1,339
Total - F4 - Sheath Wall				\$12.540
F8 - CMU Shear Wall				
F8 - 1A/CR-15 Provide (N) CMU shear wall (8 in. CMU typ uno.) adjacent to (E) wall 1A/CR-15				
Continuous 12"Wx12"H concrete cap on new CMU wall	4	CV	\$597.79	\$2,139
(2) 3/4" dia stud embeds welded to US of (E) steel beam	22	ea	\$3.87	\$85
L4x4x5/16 x 8' diagonal bracing welded each end	2,024	lb	\$4.12	\$8,339
F8, 8" wall, 17' high				
Provide (N) CMU shear wall (8 in. CMU typ uno.) adjacent to (E) wall	2,992	sf	\$34.25	\$102,476
At (E) steel column, weld horiz bars to tie to new CMU wall, typ.	176	lf	\$4.12	\$725
F8-A				
Salvage and reinstall miscellaneous electrical outlets, switches, data outlets, fire	140	ıc	¢50.00	¢7.450
alarm devices.	149	lî of	\$50.00	\$7,450 ¢660
Remove 2x4 celling panels and grid back 5 reet.	590	SI	<b>ΦΙ.ΙΙ</b>	\$00Z
fonting	596	sf	\$5 69	\$3 391
Salvage plastic laminate wainscot panels and demolish aluminum trim.	2.533	sf	\$0.35	\$887
Demolish existing gypsum board finish on one side of wall and construct adjacent	_,	•	,	<b>,</b>
CMU wall per structural.	2,533	sf	\$0.60	\$1,520
Install metal furring with painted gypsum board finish.	2,533	sf	\$13.15	\$33,309
Reinstall 2x4 ceiling system.	596	sf	\$5.15	\$3,069
Patch and polish concrete floor.	596	sf	\$22.44	\$13,374
Reinstall plastic laminate wainscot panels and install new aluminum trim	2,533	sf	\$1.05	\$2,660
F8-B				
Demolish decorative brick pier	1	ea	\$510.00	\$510
Install new decorative brick pier after completion of new shear wall	1	ea	\$1,700.00	\$1,700
Element	Quantity	Unit	Unit Cost	Total
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F8-C				
Salvage and reinstall miscellaneous electrical outlets, switches, data outlets, fire				
alarm devices.	68	lf	\$50.00	\$3,400
Remove 2x4 ceiling panels and grid back 3 feet.	272	sf	\$1.11	\$302
Sawcut and remove concrete floor slab along length of wall. Excavate for new	272	of	\$5.60	¢1 5/8
Demolish existing gypsum board finish on one side of wall and construct adjacent	212	51	ψ5.09	ψ1,540
CMU wall per structural.	1,156	sf	\$0.60	\$694
Install metal furring with painted gypsum board finish.	1,156	sf	\$13.15	\$15,201
Reinstall 2x4 ceiling system.	272	sf	\$5.15	\$1,401
Patch carpeting	272	sf	\$5.55	\$1,510
Total - F8 - CMU Shear Wall				\$206,350
R5 - Out-of-Plane Connection under Metal Deck				
R5				
New out-of-plane connection and continuity ties (3 x 3 x 1/4 angle at 8 ft max	10.005		<b>*</b> 4 4 0	<b>*</b> 4 4 <b>-</b> 0 0
spacing) At underside of metal deck.	10,825	lb	\$4.12	\$44,598
I/CR-19 (1) at each R5 location				
(1) $1.3x3x1/4 \times 8'$ long angles, welded each end	2.344	lb	\$4,12	\$9,658
(1) PL3/8 x 12"x6" welded to truss top chord	458	lb	\$4.12	\$1,886
(1) PL1/2 x 12"x6"	611	lb	\$4.12	\$2,515
(1) PL3/8 x 6"x6" knife plate w/ (2) 7/8" drilled holes, welded to 12x6 plate	229	lb	\$4.12	\$943
(2) 3/4" epoxy anchors	104	ea	\$29.98	\$3,118
R5 - 1/CR-17				
1/CR-17				
Per location				
PL1/2 x 12"x48" (assumed) welded to HSS, w/ (24) 7/8" holes	282	lb	\$4.12	\$1,161
Pack grout into cells in wall	3	IS	\$150.00	\$450
(24) 3/4" epoxy anchors into grout	12	ea	\$29.98	\$2,159
R5 - 1/CR-21				
1/CR-21				
(1) location total	1		¢сод до	<b>ሰ</b> ር ጋር
Continuous 8"WX I2"H concrete cap on new CMU wall	1	cy	\$597.79 ¢3.87	۵25¢ دی
(2) 5/4 uid stud embeds welded to US of (E) steel beam	0 736	ea Ih	ቆጋ.07 \$1 12	¢3 U33
	750	U	ψ4.12	ψ0,002
R5-A				
Demolish hard lid ceiling and 1x1 acoustical tiles (where occurring). Remove and			<b>*</b> · ·-	▲ / == -
salvage lighting for access to underside of roof deck.	394	sf	\$4.45	\$1,753
Install steel members at underside of root deck per structural (see above)				
raton cening, install new TXT acoustical tiles (where occurring), and reinstall	201	cf	<b>ድ</b> ጋጋ 10	ሮ፬ 7ቦታ
າຍາາແກຍ.	594	51	φ <b>ΖΖ.</b> ΙU	φ0,/0/

Element	Quantity	Unit	Unit Cost	Total
R5-B Remove and salvage 2x4 ceiling panels. Disassemble ceiling grid and salvage				
lighting as necessary for structural work.	13,528	sf	\$2.23	\$30,167
Reinstall 2x4 ceiling system and lighting	13,528	sf	\$9.15	\$123,781
Remove and replace grilles, registers, and diffusers outlets with new including flex duc	t 394	sf	\$1.85	\$729
R&R grilles, registers, and diffusers outlets	13,528	sf	\$0.95	\$12,852
R&R Electrical allowance in ceiling R5-A	394	sf	\$11.00	\$4,334
R&R Electrical allowance in ceiling R5-B	13,528	sf	\$5.00	\$67,640
Total - R5 - Out-of-Plane Connection under Metal Deck				\$320,042
R6 - HSS Drag Tie				
R6			• / / •	
New HSS 3 1/2 x 2 1/2 x 3/8 (assumed) drag tie at underside of metal deck. 2/CR-21	3,079	lb	\$4.12	\$12,686
Continuous 8"Wx8"H concrete cap on new CMU wall	4	су	\$597.79	\$2,381
(2) 3/4" dia stud embeds welded to US of new R6 HSS drag beam @ 2' OC	220	ea	\$3.87	\$851
L4x4x5/16 x 8' diagonal bracing welded each end @ 8' OC	5,152	lb	\$4.12	\$21,226
R6 - 2/CR-15				
New HSS 3 1/2 x 2 1/2 x 3/8 (assumed) drag tie at underside of metal deck. 2/CR-15	518	lb	\$4.12	\$2,133
PL1/2 x 3"x6" (assumed) steel tabs, w/ 7/8" holes welded to HSS 2' OC	56	lb	\$4.12	\$230
3/4" epoxy anchors to concrete walls, 2' OC	19	ea	\$29.98	\$570
R6				• · · · ·
New HSS 3 1/2 x 2 1/2 x 3/8 (assumed) drag tie at underside of metal deck. 4/CR-21	392	lb	\$4.12	\$1,615
Continuous 8"Wx8"H concrete cap on new CMU wall	1	су	\$597.79	\$303
(2) 3/4" dia stud embeds welded to US of new R6 HSS drag beam @ 2' OC	28	ea	\$3.87	\$108
Total - R6 - HSS Drag Tie				\$12 102
				<del>- φ4</del> 2,103

Element	Quantity	Unit	Unit Cost	Total
R7 - Angle under HSS Drag				
B7				
New 2 1/2 x 2 1/2 x 1/4 steel angle at underside of HSS drag to support drag (at 8 ft max spacing). Weld angles to underside of top chord of (E) truss joist 3/CR-21				
At each R7 location (10) If L2 1/2x2 1/2x/14, welded to HSS and to US of truss top chord each	0.40		<b>*</b> 4.40	<b>\$2.00</b> 5
end	943	ID	\$4.12	\$3,885
Total - R7 - Angle under HSS Drag				\$3,885
R8 - R&R Roofing to Weld Metal Deck to Steel Members				
R8				
Remove roofing and weld (E) deck to new steel members @ 12 in. o.c.	14,365	sf	\$5.68	\$81,593
R8 1/CR-19				
1/CR-19			<b>A</b> ( ) ( <b>A</b>	<b>.</b>
(1) L3x3x1/4 x 8' long angles, welded each end	349	lb	\$4.12	\$1,439
(1) PL3/8 X 12"X6" weided to truss top chord	35	ID Ih	\$4.12 ¢4.12	\$145 ¢102
(1) PL I/2 X 12"X0" (1) DL 2/8 x 6"x6" knife plote w/ (2) 7/8" drilled beloe, welded to 12x6 plote	47	ID Ih	\$4.1Z ¢4.12	\$193 ¢72
(1) PLS/8 X 8 X 8 Kinie plate w/ (2) 7/8 drilled holes, welded to 12X8 plate (2) 3/4" epoxy anchors	8	ea	\$4.12 \$29.98	\$73 \$240
R8 1/CR-20				
1/CR-20				
(2) locations total				
New steel brackets @ 4' OC, approximately 1'x1'-6"	86	lb	\$4.12	\$355
Epoxy bolt to tilt-up wall	34	ea	\$29.98	\$1,019
Weld to US of beam	17	ea	\$24.58	\$418
R8-B				
Salvage and reinstall rooftop mechanical equipment and roof drains.	14,365	sf	\$5.00	\$71,825
Demolish roofing to steel deck and weld deck to steel members per structural. Patch roof with new deck sheathing, vapor retarder, insulation (match existing R-	14,365	sf	\$5.68	\$81,593
18 thickness), cover board, and 2-ply SBS roofing	14,365	sf	\$22.40	\$321,776
R&R AC units for new roofing	14,365	sf	\$0.80	\$11,492
R&R roof drains and flashing at pipe penetrations	14,365	sf	\$0.55	\$7,901
R&R Electrical on roof	14,365	sf	\$6.00	\$86,190
Total - R8 - R&R Roofing to Weld Metal Deck to Steel Members				\$6 <u>66,253</u>

Element		Unit	Unit Cost	Total
N1 - Bracing above Ceiling at Interior Brick Pilaster				
N1				
At interior brick pilaster without steel column, provide bracing above ceiling	973	lb	\$4.12	\$4,009
Remove and salvage 2x4 ceiling panels for access above ceiling.	112	sf	\$0.15	\$17
Install bracing at brick pilaster per structural (see above) Reinstall 2x4 ceiling panels	112	sf	\$0.62	\$69
Total - N1 - Bracing above Ceiling at Interior Brick Pilaster				\$4,096
N3 - Fire Suppression Piping Seismic Bracing				
N3-A				
Remove and salvage 2x4 ceiling panels for access above ceiling. At hard lid	66 069	of	¢0.15	¢0 010
Install sprinkler system bracing per structural	66,068	si	\$0.15 \$1.37	\$9,910
Reinstall 2x4 ceiling panels. At hard lid ceilings, patch access holes to match			<b>AA AA</b>	<b>*</b> 40.000
existing finishes At 2x4 grid ceilings, install oversized escutcheons at sprinkler head penetrations	66,068 66,068	st sf	\$0.62 \$0.98	\$40,962 \$64,747
Total - N3 - Fire Suppression Piping Seismic Bracing				\$206,132
N5 - Bracing at Interior Masonry Walls and Partitions				
Bracing at interior masonry walls and partitions - allowance	66,068	sf	\$0.50	\$33,034
Total - N5 - Bracing at Interior Masonry Walls and Partitions				\$33,034
N6 - Brace Tall Narrow Contents				
Brace tall narrow contents - allowance	66,068	sf	\$0.25	\$16,517
Total - N6 - Brace Tall Narrow Contents				\$16,517
N7 - Brace/Anchor Fall-Prone Contents over 20 lbs				
Brace/anchor fall-prone contents over 20 lbs - allowance	66,068	sf	\$0.10	\$6,607
Total - N7 - Brace/Anchor Fall-Prone Contents over 20 lbs				\$6, <u>607</u>

Element	Quantity	Unit	Unit Cost	Total
N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs				
Brace/anchor fall-prone equipment over 20 lbs - allowance	66,068	sf	\$0.15	\$9,910
Total - N8 - Brace/Anchor Fall-Prone Equipment over 20 lbs				\$9,910
N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High				
Brace/anchor tall narrow equipment over 6 ft high - allowance	66,068	sf	\$0.15	\$9,910
Total - N9 - Brace/Anchor Tall Narrow Equipment over 6 ft High				\$9,910
N10 - Brace in-Line Equipment over 75 lb				
Brace in-line equipment over 75 lb - allowance	66,068	sf	\$0.20	\$13,214
Total - N10 - Brace in-Line Equipment over 75 lb				\$13,214
N14 - Brace Fluid and Gas Piping				
Pipe bracing	66,068	sf	\$0.20	\$13,214
Total - N14 - Brace Fluid and Gas Piping				\$13,214
N15 - Brace Ducts Larger Than 6 sf Cross-Section				
Duct bracing	66,068	sf	\$0.20	\$13,214
Total - N15 - Brace Ducts Larger Than 6 sf Cross-Section				\$13,214
Hazmat Abatement Allowance				
Hazmat abatement allowance	66,068	sf	\$2.50	\$165,170
Total - Hazmat Abatement Allowance				\$165,170

Project # 22-00165.02 03/18/22

Building Part D

### SUMMARY - BUILDING PART D

Element		Total	Cost / SF	
01 06 07	F1 - Connect Tilt-up Walls to Foundations F6 - Anchor Columns F7 - Strengthen Portal Frames		\$300 \$720 \$3,896	\$0.04 \$0.09 \$0.48
	Subtotal General Conditions	10.00%	\$4,916 \$492	\$0.61 \$0.06
	Subtotal General Requirements	4.00%	\$5,407 \$216	\$0.67 \$0.03
	Subtotal Bonds & Insurance	2.00%	\$5,623 \$112	\$0.69 \$0.01
	Subtotal Contractor's Fee	5.00%	\$5,736 \$287	\$0.71 \$0.04
	Subtotal Design Contingency	20.00%	\$6,023 \$1,205	\$0.74 \$0.15
	Subtotal Escalation to MOC, 08/15/23	8.99%	\$7,227 \$650	\$0.89 \$0.08
Т	OTAL ESTIMATED CONSTRUCTION COST		\$7,877	\$0.97

Total Area:

8,100 SF

Prepared by  $C\overline{UMMING}$ 

Element	Quantity	Unit	Unit Cost	Total
F1 - Connect Tilt-up Walls to Foundations				
F1 Remove and reinstall bench	2	ea	\$150.00	\$300
Total - F1 - Connect Tilt-up Walls to Foundations				\$300
F6 - Anchor Columns				
F6 At base of (E) columns at covered play area, provide two new anchor bolts. drill & epoxy into (E) foundation F6-A Paint bolts where exposed to view	16	ea ea	\$37.47 \$7.50	\$600 \$120
Total - F6 - Anchor Columns				\$720
F7 - Strengthen Portal Frames				
<ul> <li>F7</li> <li>At (E) portal frames, provide new steel plates and welds to strengthen portal frame moment connections</li> <li>F7-A</li> <li>Remove paint from existing steel structure where new steel plates are to be installed.</li> <li>Paint new steel plates</li> </ul>	800 40 40	lb If If	\$4.12 \$10.00 \$5.00	\$3,296 \$400 \$200
Total - F7 - Strengthen Portal Frames				\$3,896